

**EXPERIMENTAL STUDIES ON THE
NONLINEAR VIBRATIONS OF BEAMS AND
CYLINDRICAL SHELLS**

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EXPERIMENTAL STUDIES ON THE NONLINEAR VIBRATIONS OF BEAMS AND CYLINDRICAL SHELLS

by

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Submitted

in fulfillment of the requirements of the degree of Doctor of Philosophy

to the



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Certificate

This is to certify that the thesis entitled “**Experimental Studies on the Nonlinear Vibrations of Beams and Cylindrical Shells**” being submitted by **Mr. Ajay Kumar** to the Indian Institute of Technology Delhi for the award of degree of **Doctor of Philosophy** in Applied Mechanics is a record of original, bonafide research work carried out by him under my supervision and guidance. The thesis work, in my opinion, has reached the requisite standard fulfilling the requirements for the degree of Doctor of Philosophy.

The results contained in this thesis have not been submitted in part or in full, to any other university or institute for the award of any degree or diploma.

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(Ajay Kumar)

Abstract

The thin walled straight/curved beams and circular/noncircular cylindrical shells undergoing vibrations with amplitude of the order of their thickness or greater depict a significant effect of geometric nonlinearity involving traveling wave response, external resonances at forcing frequencies away from linear free vibration frequencies, internal resonance, participation of sub-or super-harmonics, quasi periodic and chaotic responses among the other nonlinear vibration characteristics. The experimental investigations on the nonlinear vibration of structures are important to validate their numerical prediction and to explore new phenomena/modal interactions.

The thesis deals with the nonlinear vibration of inextensional cantilever beams with accurate representation of curvature/inertia nonlinearities/spatial discretization, response of curved beams under symmetric/anti-symmetric excitation, experimental study of large amplitude vibrations of cantilever circular cylindrical shells and investigation of travelling wave response, and the study on the nonlinear response of elliptical cylindrical shell under harmonic excitation through experiments.

An experimental set-up involving non-contact harmonic excitation of beams/shells, acceleration measurement and data processing system is employed for the nonlinear vibration study of cantilever, curved beams, circular and noncircular cylindrical shells made up of aluminum. The nature of traveling wave response in cylindrical shells is investigated using a series of accelerometers along the circumference/high speed cameras. The periodic response of inextensible straight cantilever beams and curved beams is also investigated numerically using finite element and shooting technique coupled with the Newmark's direct time integration and arc length continuation.

The nonlinear response of cantilever beams depicts mild hardening for the first mode and the increasing degree of softening nonlinearity for second/higher modes. The third order approximation of nonlinear inertia/curvature terms leads to smaller hardening and softening for first and second/third modes, respectively. The single mode approximation of transverse displacement leads to significantly greater degree of hardening for first mode, smaller degree of softening for second and greater degree of softening nonlinearity for fourth mode compared to more accurate solution. The coupled mode response involving symmetric and anti-symmetric modes is observed for the direct excitation of both symmetric and anti-symmetric modes of fixed-fixed curved beams.

The cantilever circular cylindrical shell depicts increasing degree of softening nonlinearity for excitation in the neighbourhood of modes with increasing number of circumferential waves, and the travelling wave response is observed for modes with circumferential wave number equal to 3 and 5.

The elliptical cylindrical shell depicts softening nonlinearity, travelling waves over part of the circumference or along the full circumference with/without variable amplitude depending upon the forcing frequency. The participation of different modes involving 1:1, 2:1, 3:1 external, 1:1, 1:2, 2:3 internal resonances and the presence of harmonics including multiples of $1/2$, $1/3$ are reported. For the excitation of the elliptical cylindrical shell between semi minor and major axes, the response is found to be predominantly travelling wave type for a greater range of excitation frequency.

सारांश

अपनी मोटाई के प्रमाण आयाम से कंपन कर रही पतली सरल / वक्राकार पट्टियाँ एवं बेलनाकार खोल, असमानुपातिक विकृति-विस्थापन संबंध का महत्वपूर्ण प्रभाव जैसे

परिधीय दिशा मे प्रगामी तरंग व्यवहार, अरेखीय आज़ाद कंपनी की आवृत्तियों से भिन्न आवृत्ति वाले बाह्य बलों के अधीन अनुनाद, आंतरिक अनुनाद, भिन्नांक/ पूर्णांक हारमोनिक्स की सहभागिता, लगभग पुनरावृत्त एवं अव्यवस्थित कंपनी आदि अरेखीय कंपनी विशेषताओं को दर्शाते हैं। संरचनाओं के अरेखीय कंपनी का प्रायोगिक अध्ययन, अभिकलनात्मक अनुमानों के प्रमाणन एवं नये प्रकार के व्यवहार, विभिन्न आज़ाद कंपनी रूपों के पारस्परिक प्रभाव की खोज आदि करने की दृष्टि से महत्त्वपूर्ण है।

प्रस्तुत शोध प्रबंध, अखिंचनीय केंद्रीय अक्ष वाली कैन्टीलीवर पट्टी का अरेखीय कंपनी, अरेखीय वक्रता / जड़त्व के विशुद्ध प्रतिरूप / स्पेशियल अंतर्वेशन के साथ, मध्य बिन्दु के सापेक्ष सममित / असममित बलों के अधीन वक्राकार पट्टियों का कंपनी व्यवहार, कैन्टीलीवर वृत्तीय बेलनाकार कोश के बृहद् आयामीय कम्पनों का प्रायोगिक अध्ययन एवं प्रगामी तरंग व्यवहार का अन्वेषण तथा दीर्घवृत्तीय बेलनाकार कोश का सन्नादी बाह्य बलों के अधीन अरेखीय कंपनी व्यवहार का प्रायोगिक अध्ययन प्रस्तुत करता है।

एल्युमीनियम से निर्मित कैन्टीलीवर, वक्राकार पट्टी, वृत्तीय एवं दीर्घवृत्तीय बेलनाकार कोशों के अरेखीय कंपनी व्यवहार के अध्ययन के लिये अस्पर्शी आवर्ती उत्तेजन, त्वरण मापन एवं प्रक्रियण प्रणालियों का उपयोग किया गया है। बेलनाकार कोशों में प्रगामी तरंग व्यवहार का अध्ययन, परिधीय दिशा में त्वरणमापियों की एक शृंखला एवं द्रुतगतीय प्रतिबिम्बमापी के द्वारा किया गया है। अखिंचनीय केंद्रीय अक्ष वाली कैन्टीलीवर

एवं वक्राकार पट्टियों के आवर्ती कंपन व्यवहार का अध्ययन अल्पांश, शूटिंग तकनीक, न्यूमार्क की अंकगणितीय समय समाकलन एवं बहुआयामी चाप लम्बाई सांतत्य विधियों के प्रयोग से अन्वेषित किया गया है।

कैन्टीलीवर का अरेखीय कंपन व्यवहार, प्रथम विधा में सूक्ष्म कठोर प्रकृति एवं द्वितीय/ उच्च विधाओं में बढ़ती नरम प्रकृति दर्शाता है। अरेखीय जड़त्व / वक्रता का त्रिघातीय सन्निकटन प्रथम तथा द्वितीय / तृतीय विधाओं में क्रमशः कठोर एवं नरम व्यवहार में कमी दर्शाता है। अनुप्रस्थ विस्थापन का एकल विधा सन्निकटन परिशुद्ध हल की तुलना में, प्रथम विधा में कठोरता में प्रचुर वृद्धि, द्वितीय विधा में नरमता में कमी एवं चतुर्थ विधा में नरमता में वृद्धि दर्शाता है। मध्य बिन्दु के सापेक्ष सममित एवं असममित विधाओं का समिश्रित व्यवहार, वक्राकार पट्टियों के सममित एवं असममित विधाओं के उत्तेजन में पाया गया है।

कैन्टीलीवर वृत्तीय बेलनाकार कोश, परिधीय तरंग क्रम बढ़ने के साथ बढ़ती हुयी अरेखीय नरम व्यवहार तथा परिधीय तरंग क्रम 3 और 5 के लिए प्रगामी तरंग व्यवहार दर्शाती है।

दीर्घवृत्तीय बेलनाकार कोश, नरम अरेखीय व्यवहार, बाह्य उत्तेजक बल की आवृत्ति पर निर्भर परिधीय अल्पांश/ पूर्ण परिधि में प्रगामी तरंगें स्थिर / बदलते आयाम के साथ दर्शाती है। विभिन्न विधाओं की सहभागिता 1:1, 2:1, 3:1 बाह्य एवं 1:1, 1:2,

2:3 आंतरिक अनुनादों के कारण तथा विभिन्न (पूर्णांक (1,2,3,...) / भिन्नांक (1/2, 1/3

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प्रगामी तरंग व्यवहार बड़े उत्तेजन आवृत्ति परिसर में पाया गया है।

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Nomenclature

English Notations

A	:	Area
A_i ($i = 0, 1, 2, \dots$)	:	Harmonic amplitude
b	:	Width of beams
C	:	Circumferential length of shells
$\mathbf{d}, \dot{\mathbf{d}}, \ddot{\mathbf{d}}$:	Displacement, velocity and acceleration vectors
\mathbf{d}_i	:	Vector of elemental degrees of freedom of i^{th} element
\mathbf{D}	:	Global damping matrix
$\tilde{\mathbf{D}}$:	Modal damping matrix
\mathbf{D}^i	:	Elemental damping matrix
E	:	Young's modulus
\mathbf{F}	:	Global load vector
\mathbf{F}^i	:	Elemental load vector
$\tilde{\mathbf{F}}$:	Modal load vector
h	:	Mean thickness
\mathbf{H}	:	Vector of Hermite interpolation functions
$\mathbf{H}_{,i}, \mathbf{H}_{,j}$:	$\frac{\partial \mathbf{H}}{\partial x_i}, \frac{\partial \mathbf{H}}{\partial x_j}$
$\mathbf{H}_{,ii}$:	$\frac{\partial^2 \mathbf{H}}{\partial x_i^2}$

I	:	Area moment of inertia about y axis
\mathbf{I}	:	Identity matrix
\mathbf{K}	:	Global stiffness matrix
\mathbf{K}_{NL}	:	Nonlinear stiffness matrix
$\mathbf{K}_1^i, \mathbf{K}_2^i, \mathbf{K}_3^i$:	Elemental stiffness matrices
$\mathbf{K}_4^i, \mathbf{K}_5^i, \mathbf{K}_6^i$:	
$\tilde{\mathbf{K}}$:	Modal stiffness matrix
L	:	Mean Length
l_i	:	Length of ith element
\mathbf{M}	:	Global mass matrix
$\mathbf{M}_1^i, \mathbf{M}_2^i$:	Elemental mass matrices
$\tilde{\mathbf{M}}$:	Modal mass matrix
R	:	Radius
\mathbf{R}	:	Global internal and inertia force vector
\mathbf{R}_i	:	Elemental internal and inertia force vector
$\tilde{\mathbf{R}}$:	Modal internal and inertia force vector
t	:	Time
T	:	Time period
\tilde{T}	:	Kinetic energy
u, w	:	Longitudinal and transverse displacements
u_0, w_0	:	Longitudinal and transverse mid surface displacements

\dot{u}, \dot{w}	:	Longitudinal and transverse velocity
V	:	Potential energy
$w_{,x}, w_{,xx}$:	$\frac{\partial w}{\partial x}, \frac{\partial^2 w}{\partial x^2}$
$w_{,i}, w_{,ii}$:	$\frac{\partial w}{\partial x_i}, \frac{\partial^2 w}{\partial x_i^2}$
$w_{,j}$:	$\frac{\partial w}{\partial x_j}$
$w_{,s}$:	$\frac{\partial w}{\partial s}$
\ddot{w}	:	Transverse acceleration
$\dot{w}_{,x}$:	$\frac{\partial \dot{w}}{\partial x}$
w^i	:	Transverse displacement with in i th element
$\delta \tilde{T}$:	First variation of kinetic energy
δV	:	First variation of potential energy
δW	:	Virtual work
x	:	Longitudinal coordinate
z	:	Transverse coordinate

Greek Notations

α, β	:	Rayleigh proportional damping parameter
δ	:	Variational symbol
θ	:	Rotation of normal in sz plane of curved beam

$\tilde{\theta}$:	Angular position from excitation point in circular cylindrical shell
Δ	:	Increment in a quantity
$\boldsymbol{\eta}, \dot{\boldsymbol{\eta}}, \ddot{\boldsymbol{\eta}}$:	Modal displacement, velocity, acceleration vectors
$\tilde{\boldsymbol{\eta}}$:	State vector
$\tilde{\boldsymbol{\eta}}_0$:	initial guess of state vector
ν	:	Poisson's ratio
ω_F	:	Forcing frequency
ω_i	:	Natural frequency of i th mode
ψ_i	:	Phase angle of i th harmonics
ρ	:	Density
$\boldsymbol{\Phi}$:	Vector of eigen functions of linear free vibration modes of cantilever beam
$\boldsymbol{\Phi}_{,x}, \boldsymbol{\Phi}_{,xx}$:	$\frac{\partial \boldsymbol{\Phi}}{\partial x}, \frac{\partial^2 \boldsymbol{\Phi}}{\partial x^2}$
ξ_1, ξ_2	:	Damping factor in first anti-symmetric and symmetric modes of curved beams
$\lambda, \tilde{\delta}$:	Constants of Newmark's time integration method