

ATTRITION OF BED MATERIAL IN A RECIRCULATING FLUIDIZED BED

SHIVALI CHOURASIA



**DEPARTMENT OF CIVIL ENGINEERING
INDIAN INSTITUTE OF TECHNOLOGY DELHI
JULY 2017**

ATTRITION OF BED MATERIAL IN A RECIRCULATING FLUIDIZED BED

by

Shivali Chourasia

DEPARTMENT OF CIVIL ENGINEERING

Submitted

In fulfillment of the requirements of the degree of Doctor of Philosophy

to the



INDIAN INSTITUTE OF TECHNOLOGY DELHI

JULY 2017

CERTIFICATE

This is to certify that the thesis entitled “**Attrition of Bed Material in a Recirculating Fluidized Bed**”, being submitted by **Ms. Shivali Chourasia**, to the **Indian Institute of Technology Delhi**, for the award of ‘**Doctor of Philosophy**’ in Department of Civil Engineering is a record of the bonafide research work carried out by her under my supervision and guidance. She has fulfilled the requirements for the submission of this thesis, which to the best of my knowledge has reached the requisite standard.

The material contained in the thesis has not been submitted in part or full to any other University or Institute for the award of any other degree or diploma.

Babu J. Alappat
Professor
Department of Civil Engineering
Indian Institute of Technology Delhi
New Delhi-110016, India

Date:
New Delhi

ACKNOWLEDGEMENTS

Firstly, I would like to express my sincere gratitude to my supervisor Prof. Babu J. Alappat for giving me a chance to work under their guidance. Without his unstinted support, guidance, motivation and patience, this dream would have remained a dream. I would also like to sincerely thank him for his moral support during this journey.

I am also thankful to my SRC Members, Prof. Ashok Gupta, Dr. D. R. Kaushal and Dr. Sudip K. Pattanayek for rendering me their valuable comments, encouragement and time towards my research. I would also like to extend my gratitude to my PhD Thesis examiners Prof. Eldho T. I. and Prof. Pascaline Pre for their efforts and valuable suggestions to improve the quality of my Thesis. A special note of gratitude to Dr. Sanjay Gupta, Mr. Ishwar Singh and Mr. Shiv Shankar Shukla for their valuable support in the lab.

I would also like to thank the present HOD of Civil Engineering Department Prof. Manoj Dutta and former HODs, Prof. A. K. Gosain, and Prof. Arvind Jain. My sincere gratitude goes to Mr. Rajveer Aggarwal, Mr. Vikram, Mr. Randhir Jha, Mr. Amit Bundela, Mrs. Neeru Sharma, Mrs. Pooja Anand, Mr. Nena Ram Gehlot, Mr. Jeetram and other staff members of the Civil Engineering Department for their assistance.

I would also like to thank all faculty members of Environmental Engineering Prof. M. K. Khare, Prof. A. K. Nema, Dr. Gazala Habib, and Dr. Arun Kumar for their support.

I would like to thank the Textile Department for assisting in the SEM analysis of the samples.

My genuine thanks to all my friends especially Ms. Isha Khanna, Ms. Tropita Piplai, Mr. Sumanth Chinthala, Mrs. Roshni Mary, Mr. Prateek Negi, Mrs. Aali Pant and Mr. Gaurav Manchanda for all the stimulating discussions, support and fun we have had in the last five years.

A special thanks to my family. My parents, Mr. Om Prakash and Mrs. Sandhya Chourasia for always standing by me during my highs and lows throughout my life and motivating me to achieve all my dreams. I would like to extend my gratitude to my sister, Mrs. Vaishali Sharma; brother in law, Mr. Anand Sharma; my niece and nephew, Aadya and Geetansh for their unconditional love and affection and Mr. Abhilash Shukla for all the love, support and encouragement. All their support have always been and will always be crucial to my personal life as well as my career endeavours.

Lastly, I am grateful to God for everything.

Shivali Chourasia

ABSTRACT

The fluidized bed is one of the best known contacting methods used in the processing industry. Recirculating fluidized bed (RCFB) is a conventional gas-solid contactor widely used in process industries for drying, coating, catalytic conversion, combustion and gasification. Attrition is an essential concern in all types of fluidized bed operation. Attrition of solid particles caused by abrasion and fragmentation results in loss of bed material and influences the normal operation, functioning and performance of the fluidized bed reactors.

The objective of this study was the investigation of the attrition of sand particles (Geldart D) in a RCFB. The idea was to investigate the effects of various parameters like superficial air velocity of the fluidizing air, bed inventory and spacing between jet top and draft tube bottom (spacer height) on the attrition of bed material and their size distribution with increasing operation time and to propose a methodology to estimate the attrition of sand particles in a RFCB. The effects of attrition of bed material on the solid circulation rate was also investigated in detail.

Experiments were performed at ambient conditions, with superficial air velocity ranging from 7.13 m/s to 9.16 m/s, bed inventory of 7 kg to 10 kg, spacing of 0.085 m and 0.045 m between jet top and draft tube bottom for an operation time of 40 hours. Bed material was prepared from Indian Standard (IS) Grade I sand using sieves of size 2.2 mm and 1.0 mm. It was found that, with increasing operation time and other parameters (bed inventory, superficial air velocity, and spacer height), attrition of bed material was also increasing. Generation and elutriation of fines were significant at higher superficial air velocity, bed inventory and spacer height. Further, qualitative characterization was done through SEM for the confirmation of mode of attrition of

the particles. Mode of the attrition of particles was found to be abrasion rather than fragmentation.

Particles of the size less than 300 μm were found to be escaping from the reactor with the fluidizing air. This corresponds to the material loss due to the attrition of bed material during operation. The amount of the material lost after 40 hours of operation with the superficial air velocity of 9.16 m/s for 10 kg inventory was around 7.28% of the total bed inventory. For the same scenario, decreasing the superficial air velocity to 8.15 m/s brought down the material loss to about 6.88%.

Effects of attrition of bed material on the solid circulation rate were studied in detail. A mathematical model was developed on the basis of the experimental results to identify the effects of attrition of bed particles on the solid circulation rate incorporating the effects of the various operating and design parameters. To develop the model, dimensional analysis and nonlinear regression were used. The model equation was a nonlinear equation which implies the relationship between the solid circulation rate and the operating and design parameters. The model equation can estimate the solid circulation rate over a range of operation time and other parameters. Decrease in solid circulation rate with increasing operation time can be predicated, using this model equation.

A methodology was proposed to estimate the mass of fines generated in an RCFB by summing up separately the estimated fines generated in the downcomer (bubbling bed attrition) and in the draft tube (jet induced attrition). The total material loss obtained from the experimental results was compared with the mass of generated fines estimated using the models. The proposed methodology can be helpful in the scaling of RCFB reactor and to calculate the total material loss and fines generation in the reactor.

This study provides a detailed analysis of the attrition of sand particles in a recirculating fluidized bed and would help estimate the amount of material loss due to attrition of bed material.

Keywords: Fluidization, Attrition, Elutriation, Material loss, Solid circulation rate, Jet-induced attrition, Bubbling bed attrition

सार

प्रसंस्करण उद्योग में उपयोग किए जाने वाले सबसे प्रसिद्ध संपर्क तरीकों में से एक द्रवीकृत बैड है। द्रवीकृत बैड (आर.सी.एफ.बी.) पुनरावृत्ति एक पारंपरिक गैस-ठोस संपर्कक है, जो सूखने, कोटिंग, उत्प्रेरक रूपांतरण, दहन और गैसीकरण के लिए प्रक्रिया उद्योगों में व्यापक रूप से उपयोग किया जाता है। सभी प्रकार के द्रवयुक्त बैड ऑपरेशन में एट्रिशन एक अनिवार्य चिंता है। घर्षण और विखंडन के परिणामस्वरूप ठोस कणों का घूमना बैड सामग्री के नुकसान में होता है और सामान्य ऑपरेशन, कामकाज और द्रवयुक्त बैड रिएक्टरों के प्रदर्शन को प्रभावित करता है। इस अध्ययन का उद्देश्य आरसीएफबी में रेत कणों (गेल्डर्ट डी) के उन्मूलन की जांच थी। यह विचार विभिन्न मापदंडों के प्रभावों की जांच करना था जैसे द्रव वायु, बैड सामग्री और जेट शीर्ष और मसौदा ट्यूब तल (स्पेसर ऊँचाई) के बीच बैड सामग्री के उन्मूलन और उनके संचालन के समय में वृद्धि के साथ और आकार वितरण के बीच अंतर। एक आरएफसीबी में रेत के कणों के उन्मूलन का अनुमान लगाने के लिए एक पद्धति का प्रस्ताव ठोस परिसंचरण दर पर बैड सामग्री के टूटने का प्रभाव भी विस्तार से जांच की गई।

7.13 एम /एस से 9.16 एम /एस तक की सतही वायु वेग, 7 किलोग्राम से 10 किलोग्राम की बैड सूची, 0.085 मीटर और 0.045 मीटर की दूरी पर जेट शीर्ष के बीच की दूरी और एक ऑपरेशन समय 40 घंटे के लिए ड्राप ट्यूब के तल पर परिवेश की स्थिति पर प्रयोग किया गया। बैड सामग्री 2.2 मिमी और 1.0 मिमी आकार के चलनी के जरिये भारतीय मानक (आईएस) ग्रेड I रेत से तैयार की गई थी। यह पाया गया कि, बढ़ते संचालन के समय और अन्य मापदंडों (बैड सामग्री की मात्रा, सतही वायु वेग और स्पेसर ऊँचाई) के साथ, बैड सामग्री के उन्मूलन भी बढ़ रहे थे। इसके अलावा, कणों के उन्मूलन की स्थिति की पुष्टि के लिए एस.इ. म. के माध्यम से गुणात्मक लक्षण वर्णन किया गया। कणों के उन्मूलन का मोड विखंडन की बजाय घर्षण पाया गया।

फ्लूइडिंग वायु के साथ रिएक्टर से 300 माइक्रोग्राम से कम आकार के कणों को भागने में पाया गया। यह ऑपरेशन के दौरान बैड सामग्री के घृणा के कारण सामग्री के नुकसान से मेल खाती है। 10 किलो इन्वेंट्री के लिए 9.16 एम /एस के सतही वायु वेग के साथ ऑपरेशन के 40 घंटों के बाद खो जाने वाली सामग्री की मात्रा कुल बिस्तरों की सूची का 7.28% थी। इसी परिदृश्य के लिए, सतही वायु वेग में 8.15 एम /एस की कमी से सामग्री हानि को लगभग 6.88% कम कर दिया गया।

ठोस परिसंचरण दर पर बैड सामग्री के घृणा का प्रभाव विस्तार से अध्ययन किया गया। विभिन्न ऑपरेटिंग और डिजाइन मापदंडों के प्रभाव को शामिल करने वाले ठोस परिसंचरण दर पर बैड कणों के घृणा के प्रभावों की पहचान करने के लिए प्रयोगात्मक परिणामों के आधार पर एक गणितीय मॉडल विकसित किया गया था। मॉडल विकसित करने के लिए, आयामी विश्लेषण और गैर-रेखीय प्रतिगमन का इस्तेमाल किया गया था। मॉडल समीकरण एक गैर-रेखीय समीकरण था, जिसका मतलब है कि ठोस परिसंचरण दर और संचालन और डिजाइन पैरामीटर के बीच संबंध। मॉडल समीकरण ऑपरेशन समय और अन्य मापदंडों की एक श्रृंखला पर ठोस परिसंचरण दर का अनुमान

लगा सकता है। इस मॉडल समीकरण का उपयोग करते हुए, बढ़ते संचालन के समय के साथ ठोस परिसंचरण दर में कमी की जा सकती है।

डाउनॉमर (बब्ब्लिंग बैड के उन्मूलन) में उत्पन्न अनुमानित महीन कढ़ और मसौदा ट्यूब (जेट प्रेरित उन्मुक्ति) में एक आरसीएफबी में उत्पन्न महीन कढ़ के द्रव्यमान का अनुमान लगाने के लिए एक पद्धति का प्रस्ताव किया गया था। प्रयोगात्मक परिणामों से प्राप्त कुल भौतिक हानि की तुलना मॉडल के उपयोग के अनुमानित जननुमा के द्रव्यमान से की गई थी। प्रस्तावित पद्धति आरसीएफबी रिएक्टर के स्केलिंग में सहायक हो सकती है और रिएक्टर में कुल भौतिक हानि और महीन कढ़ की गणना करने के लिए।

TABLE OF CONTENTS

Certificate	i
Acknowledgements	ii-iii
Abstract	iv-vi
Table of Contents	vii-xi
List of Figures	xii-xvi
List of Tables	xvii
Nomenclature	xviii-xix
1.0 Introduction	1-17
1.1 Introduction to Fluidization	1
1.2 History of Fluidization and Its Applications	4
1.3 Geldart Classification of Powders	7
1.4 Circulating Fluidized Bed (CFB)	8
1.4.1 The advantages of CFB	9
1.4.2 Applications of CFB	10
1.5 Spouted Bed	10
1.6 Recirculating Fluidized Bed (RCFB)	12
1.6.1 Advantages of RCFB	15
1.6.2 Applications of RCFB	15
1.7 Attrition in Fluidized Bed Systems	16
1.7.1 Abrasion	16
1.7.2 Fragmentation	16
1.8 Motivation for the Present Study	17
2.0 Attrition: An Overview	18-37
2.1 Introduction to Attrition	18
2.2 Modes of Attrition	19
2.3 Factors Affecting the Attrition	20

2.3.1 Attrition due to properties of particle	21
2.3.2 Attrition due to properties of surrounding of particles/process conditions	23
2.4 Assessment of Attrition	26
2.4.1 By assessment of strength of material	26
2.4.2 By assessment of the attrition induced material loss	26
2.4.3 By assessment of changes in the particle size distribution	27
2.5 Sources of Attrition in a Fluidized Bed System	27
2.5.1 Grid jet as a source of attrition	28
2.5.2 Bubble induced attrition	32
2.5.3 Cyclone as attrition source	33
2.6 Attrition in Internally Circulating Fluidized Bed (ICFB) and Spouted Bed	34
2.7 Inferences from the Literature Review	35
2.8 Objectives and Scope	36
2.8.1 Objectives	36
2.8.2 Scope	37
3.0 Experimental Methodology and Materials	38-56
3.1 Experimental Setup	38
3.2 Working of RCFB and General Methodology	43
3.3 Bed Material	45
3.4 Operating and Design Variables	48
3.5 Measurements and Computations	49
3.5.1 Pressure drop measurements	49
3.5.2 Solid circulation rate	50
3.5.3 Sieve analysis	50
3.5.4 SEM analysis	54
3.5.5 Gas bypass calculations	56
4.0 Effects of Various Parameters on the Attrition of Bed Material	57-114
4.1 General	57
4.2 Effect of Operation Time on the Attrition of Bed Material	58

4.2.1 Effect of operation time on size distribution of bed material	58
4.2.2 Effect of operation time on the harmonic diameter and effective size of particles	65
4.2.3 Effect of operation time on the coefficient of uniformity and coefficient of curvature	66
4.3 Effects of Superficial Air Velocity on Attrition of Bed Material	67
4.3.1 Effect of superficial air velocity on particles size distribution of bed material and material loss	67
4.3.2 Effect of superficial air velocity on harmonic diameter, coefficient of uniformity and coefficient of curvature	77
4.4 Effect of Bed Inventory on the Attrition of Bed Material	82
4.4.1 Effect of bed inventory on particles size distribution of bed material and material loss	82
4.4.2 Effect of bed inventory on harmonic diameter, coefficient of uniformity and coefficient of curvature	91
4.5 Analysis of the Surface Morphology Using SEM	95
4.6 Effect of Spacing between Jet Top and Draft Tube Bottom (Spacer Height) on the Attrition of Bed Material	99
4.6.1 Effect of spacer height on %weight of particles of different sizes and material loss with three different superficial air velocities	99
4.6.2 Effect of spacer height on %weight of particles of different sizes and material loss with three different bed inventories	104
4.7 Effect of Attrition on the Voidage in the Downcomer and Riser	109
4.8 Summary	113
5.0 Effects of the Attrition of Bed Materials on Solid Circulation Rate in a RCFB	115-131
5.1 General	115
5.2 Measurement and Computation of Solid Circulation Rate	116
5.3 Effect of Attrition of Bed Material on Solid Circulation Rate	117
5.3.1 Effect of attrition on the solid circulation rate for different superficial	

air velocities	117
5.3.2 Effect of attrition on the solid circulation rate for different bed inventories	119
5.3.3 Effect of attrition on the solid circulation rate for different spacer heights	120
5.4 Modeling of Solid Circulation Rate Incorporating Attrition	124
5.4.1 Dimensional analysis	125
5.4.2 Nonlinear regression to develop model equation	127
5.5 Summary	130
6.0 Estimation of the Fines Generation and Material Loss in a RFCB	132-154
6.1 General	132
6.2 Attrition in the Downcomer	133
6.3 Attrition in the Draft Tube	140
6.4 Model Calculations	142
6.5 Variations in Bubbling Bed Attrition Rate Constant (K_b) and Material Specific Constant (C_j)	146
6.5.1 Variations in K_b with superficial air velocities and spacer heights	146
6.5.2 Variations in K_b with bed inventories and spacer heights	148
6.5.3 Variations in C_j with superficial air velocities and spacer heights	149
6.5.4 Variations in C_j with bed inventories and spacer heights	151
6.6 Validation of the Models	152
6.7 Summary	153
7.0 SUMMARY AND MAJOR FINDINGS	155-158
7.1 Summary	155
7.2 Conclusions	155
7.3 Major Research Contributions	157
7.4 Applications and Significance of the Present Study	158
7.5 Limitations of the Present Study	158
7.6 Scope for Future Study	159
References	160- 173

Appendix 1: Sieve Analysis Data for the Different Sets of Experiments	174-177
Appendix 2: Calculations of Solid Circulation Rate and Non Linear Regression Model	178-184
Appendix 3: Model Calculations to Estimate the Attrition in Downcomer and Draft Tube	185-187
Curriculum Vitae	

LIST OF FIGURES

Figure 1.1: Fluidized bed reactor	2
Figure 1.2: Various regimes of fluidized bed system	4
Figure 1.3: Geldart classification of powders for fluidizing by air	8
Figure 1.4: Typical configuration of circulating fluidized bed system	9
Figure 1.5: Classical and conventional spouted bed	12
Figure 1.6: Spouted bed with a central draft tube	13
Figure 1.7: Typical configuration a RCFB	14
Figure 1.8: Attrition mechanism	17
 Figure 2.1: Attrition modes and their effects on the particle size distribution	 20
 Figure 3.1: Recirculating fluidized bed cold model experimental facility	 39
Figure 3.2: Pictures of various sections of RCFB facility at environmental lab	42
Figure 3.3: Working of RCFB reactor	44
Figure 3.4: Schematic representation of the methodology	45
Figure 3.5: Cumulative undersize %weight particles size distribution of original sand and bed material	48
Figure 3.6: Sieves of different sizes used in sieve analysis	51
Figure 3.7: Sieve shaker machine	52
Figure 3.8: SEM facility at IIT Delhi	55
Figure 3.9: SEM specimen holder with sand samples	55
 Figure 4.1: Particle size distribution of bed material for 50 hours of operation (superficial air velocity 8.15m/s and bed inventory 8 kg)	 59
Figure 4.2: Cumulative particle size distribution of bed material for 50 hours of operation (superficial air velocity 8.15 m/s and bed inventory 8 kg)	60
Figure 4.3: Ratio of initial to later mean particle diameter as a function of time (superficial air velocity 8.15 m/s and bed inventory of 8 kg)	61

Figure 4.4: Ratio of initial to later mean particle diameter as a function of time with different superficial air velocities used	62
Figure 4.5: Ratio of initial to later mean particle diameter as a function of time with different bed inventories used	62
Figure 4.6: Effect of operation time on the %weight of particles retained 2 mm sieve and 1 mm sieve	64
Figure 4.7: Effect of operation time on the %weight of particles of size less than 1 mm	64
Figure 4.8: Variation in downcomer bed heights with operation time	65
Figure 4.9: Variation in harmonic diameter and effective size of particle with operation time	66
Figure 4.10: Effect of operation time on the coefficient of uniformity and coefficient of curvature	67
Figure 4.11: Size distribution of bed material for superficial air velocities of 7.13 m/s, 8.15 m/s and 9.16 m/s, spacer height of 0.085 m and operation time (a) 10 hours (b) 20 hours (c) 30 hours (d) 40 hours	70
Figure 4.12: Size distribution of bed material for superficial air velocities of 7.13 m/s, 8.15 m/s and 9.16 m/s, spacer height of 0.045 m and operation time (a) 10 hours (b) 20 hours (c) 30 hours (d) 40 hours	73
Figure 4.13: Effect of superficial air velocity on %weight of particles of the size less than 1 mm for 40 hours of operation and a spacer height of (a) 0.085 m (b) 0.045 m	74
Figure 4.14: Effect of superficial air velocity on %weight of particles retained on size 2 mm sieve for 40 hours of operation and a spacer height of (a) 0.085 m (b) 0.045 m	76
Figure 4.15: Effect of superficial air velocity on %material loss after 40 hours of the operation for a spacer height of (a) 0.085 m (b) 0.045 m	77
Figure 4.16: Effect of superficial air velocity on (a) harmonic diameter (b) Coefficient of uniformity (c) coefficient of curvature for a spacer height of 0.085 m	80
Figure 4.17: Effect of superficial air velocity on (a) harmonic diameter (b) Coefficient of uniformity (c) coefficient of curvature for a spacer height of 0.045 m	81

Figure 4.18: Size distribution of bed material for bed inventories of 7 kg, 8 kg and 10 kg spacer height of 0.085 m and operation time (a) 10 hours (b) 20 hours (c) 30 hours (d) 40 hours	84
Figure 4.19: Size distribution of bed material for bed inventories of 7 kg, 8 kg and 10 kg spacer height of 0.045 m and operation time (a) 10 hours (b) 20 hours (c) 30 hours (d) 40 hours	86
Figure 4.20: Effect of bed inventory on the %weight of particles of size less than 1 mm for 40 hours of operation and a spacer height of (a) 0.085 m (b) 0.045 m	88
Figure 4.21: Effect of bed inventory on %weight of particles retained on 2 mm sieve for 40 hours of operation and a spacer height of (a) 0.085 m (b) 0.045 m	89
Figure 4.22: Effect of bed inventory on %material loss after 40 hours of operation for a spacer height of (a) 0.085 m (b) 0.045 m	90
Figure 4.23: Effect of bed inventory on (a) harmonic diameter (b) Coefficient of uniformity (c) coefficient of curvature for a spacer height of 0.085 m	93
Figure 4.24: Effect of bed inventory on (a) harmonic diameter (b) Coefficient of uniformity (c) coefficient of curvature for a spacer height of 0.045 m	94
Figure 4.25: SEM images of (a) original sand (b) sand particles after 40 hour (with superficial air velocity 9.15 m/s and bed inventory 10 kg) (c) sand after 50 hours (with superficial air velocity 8.15 m/s and bed inventory 8 kg) at 40X	96
Figure 4.26: SEM images of (a) original sand (b) sand particles after 40 hour (with superficial air velocity 8.15 m/s, bed inventory 8 kg) (c) sand after 40 hours (with superficial air velocity 9.15 m/s and bed inventory 10 kg) at 20,000X	98
Figure 4.27: Effect of spacer height on %weight of particles of size less than 1 mm for superficial air velocity (a) 7.13 m/s (b) 8.15 m/s (c) 9.16 m/s with bed inventory 10 kg	101

Figure 4.28: Effect of spacer height on %weight of particles retained on 2 mm sieve for superficial air velocity (a) 7.13 m/s (b) 8.15 m/s (c) 9.16 m/s with bed inventory 10 kg	103
Figure 4.29: %Material loss for superficial air velocity 7.13 m/s, 8.15m/s and 9.16 m/s after 40 hours of operation with an inventory of 10 kg	104
Figure 4.30: Effect of spacer height on %weight of particles of size less than 1 mm for bed inventory (a) 7 kg (b) 8 kg (c) 10 kg for a superficial air velocity of 8.15 m/s	106
Figure 4.31: Effect of spacer height on %weight of particles retained on 2 mm sieve for bed inventory (a) 7 kg (b) 8 kg (c) 10 kg for a superficial air velocity of 8.15 m/s	108
Figure 4.32: %Material loss for bed inventory of 7 kg, 8 kg and 10 kg after 40 hours of operation for a superficial air velocity of 8.15 m/s	108
Figure 4.33: Variations in e_d with increasing operation time for (a) different superficial velocities (b) different bed inventories	111
Figure 4.34: Variations in e_r with increasing operation time for (a) different superficial velocities (b) different bed inventories	112
Figure 5.1: Effect of attrition on the solid circulation rate for different superficial air velocities, 40 hours of operation time and a spacer height of (a) 0.085 m (b) 0.045 m	118
Figure 5.2: Effect of attrition on the solid circulation rate for different bed inventories, 40 hours of operation time and a spacer height of (a) 0.085 m (b) 0.045 m	120
Figure 5.3: Variations in solid circulation rate for 40 hours of operation, and spacer height 1 (0.085 m) and spacer height 2 (0.045 m): (a) for a superficial air velocity of 8.15 m/s and inventory of 7 kg (b) for a superficial air velocity of 8.15 m/s and inventory of 8 kg (c) for a superficial air velocity of 8.15 m/s and inventory of 10 kg (d) for a superficial air velocity of 7.13 m/s and inventory of 10 kg (e) for a superficial air velocity of 9.16 m/s and inventory of 10 kg	124
Figure 5.4: Comparison of the experimental values of solid circulation rate	

with values of estimated using the model	129
Figure 6.1: Structure of a particle including imaginative bridges	136
Figure 6.2: Variations in the value of K_b for different superficial air velocities and a spacer height of (a) 0.085 m (b) 0.045 m	147
Figure 6.3: Variations in the value of K_b for different bed inventories and a spacer height of (a) 0.085 m (b) 0.045 m	149
Figure 6.4: Variations in the value of C_j for different superficial air velocities and a spacer height of (a) 0.085 m (b) 0.045 m	150
Figure 6.5: Variations in the value of C_j for different bed inventories and a spacer height of (a) 0.085 m (b) 0.045 m	152

LIST OF TABLES

Table 1.1: Development of fluidized bed technology	5
Table 2.1: Summary of studies reported on jet induced attrition	29
Table 2.2: Summary of studies reported on bubble induced attrition	32
Table 3.1: Comparative study of Indian Standard sand, Ennore for local river sand and Quartzanium TM sand	46
Table 3.2: Characteristics of the bed material (sieved from IS Sand- Grade I)	47
Table: 3.3: Experimental details	49
Table 5.1: Units and dimensions of the different variables	126
Table 6.1: Experimental and model values of K_b for spacer height 1	144
Table 6.2: Experimental and model values of K_b for spacer height 2	144
Table 6.3: Experimental and model values of C_j for spacer height 1	145
Table 6.4: Experimental and model values of C_j for spacer height 2	145
Table 6.5: Comparison of material loss calculated using models for experimental results	153

NOMENCLATURE

ρ_p	Density of the jet gas
n_{or}	Number of orifices in the distributor
U_p	Average velocity of the particle in downcomer
K_j	Constant that characterizes the solids susceptibility to abrasion
D_{p1}	Final diameter of the particle
U_{or}	Jet gas velocity inside an orifice
D_p	Surface mean diameter of the bed solids
ΔP	Pressure drop in downcomer
μ	Viscosity of the fluidizing air
a, b, c	Model parameter
A_d	Area of downcomer
A_r	Area of riser tube
CFB	Circulating Fluidized Bed
C_c	Coefficient of curvature
C_j	Particle-size independent material specific constant
C_u	Coefficient of uniformity
D_0	Diameter of fine particles obtained after collision
d_{or}	Diameter of the orifices
d_p	Diameter of particle
D_{p1}	Diameter of initial sand particles in the bed
e	Voidage
e_d	Operating voidage in downcomer
E_p	Young's modulus of sand particle
e_r	Operating voidage in riser tube
FCC	Fluid Catalytic Cracking
f_p	Collision frequency of the particle
H_{dt}	Operating height of spout for respect to perforated plate

H_s	Height of the bed in the riser when the air flow was suddenly cut off
i	Bed inventory
k	Coefficient of restitution for particle-particle collision
K_b	Attrition rate constant of bubbling fluidized bed
L'	Height of solid bed in downcomer
M	Constant
$m_{att,b}$	Mass attrition in dense zone
$m_{att,total}$	Material loss after operation time t
RCFB	Recirculating Fluidized Bed
SEM	Scanning Electron Microscope
t	Operation time
U_{fd}	Actual velocity of air in the downcomer
U_{pd}	Particle velocity in the downcomer
U_{pr}	Particle velocity in the riser tube
v	Superficial air velocity
W_s	Solid circulation rate
w_i	Weight of particles retained on i^{th} sieve
x	Spacing between jet top and riser tube bottom (Spacer height)
x_i	Diameter of i^{th} sieve
η	Proportion of dissipation energy cumulated to give rise to attrition
σ_p	Yield strength of sand particle
ϕ_p	Sphericity factor for sand particle

Greek Symbol

ρ	Density
Π_1, Π_2, Π_3	Dimensionless variables
λ, ϕ	Functions

Subscript

D	Downcomer
p	Particle
r	Riser tube
s	Solid