

# **DESIGN AND DEVELOPMENT OF LIGHT ELECTRIC VEHICLE CHARGERS**

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**DEPARTMENT OF ELECTRICAL ENGINEERING  
INDIAN INSTITUTE OF TECHNOLOGY DELHI  
JANUARY 2024**

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# **DESIGN AND DEVELOPMENT OF LIGHT ELECTRIC VEHICLE CHARGERS**

**by**

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**DEPARTMENT OF ELECTRICAL ENGINEERING**

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**in fulfilment of the requirements of the degree of Doctor of Philosophy**

**to the**



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## **CERTIFICATE**

It is certified that the thesis entitled “**Design and Development of Light Electric Vehicle Chargers,**” being submitted by **Mr. Jitendra Gupta** for award of the degree of **Doctor of Philosophy** in the Department of Electrical Engineering, Indian Institute of Technology Delhi, is a record of the student work carried out by him under my supervision and guidance. The matter embodied in this thesis has not been submitted for award of any other degree or diploma.

Dated: 23.01.2024

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## ABSTRACT

This work deals with the design and development of high performance chargers for the light electric vehicles (LEVs), i.e., electric two wheelers (E2Ws) and electric three wheelers (E3Ws). Several desirable performance features of LEVs chargers from consumers, manufacturers, and power suppliers' perspectives are identified and correspondingly, novel LEV chargers have been designed, analyzed, and implemented in this work. A comprehensive classification of LEV chargers based on the direction of power flow (unidirectional or bidirectional), number of power conversion stages (single or double stages), and need for isolation (nonisolated or isolated) is made in this work. Notably, a wide range of supply and battery voltage conditions are considered when designing and implementing all charger topologies to ensure a general purpose/single charging solution for different classes of LEVs. In this work, the pros and cons of transformers are comprehensively analyzed, and accordingly, different novel nonisolated charging solutions are proposed for the LEV applications. In the proposed nonisolated LEV charging solutions, the applicability of the transformerless gain adjustment techniques, is comprehensively analyzed to achieve desired performance objectives under wide AC and DC side operating conditions. Further, the impact of input-output current ripples on the filter size is explored in these charger topologies, and some novel LEV chargers with continuous input-output current characteristics and low filters size are proposed in this work.

Further, the feasibility of the bidirectional charging system for the LEVs is comprehensively assessed in this work. Correspondingly, various novel bidirectional LEV chargers with grid-to-vehicle (G2V), vehicle-to-grid (V2G), and vehicle-to-home (V2H) modes operational capabilities are proposed for ensuring greater benefits to the LEVs consumers and power suppliers. Further, the seamless mode transfer capability of proposed bidirectional LEV chargers under grid disconnection and reconnection events, is critically analyzed, and correspondingly, a simple yet robust control framework is formulated to achieve desired performance characteristics under normal/abnormal operating conditions.

Notably, all the proposed unidirectional and bidirectional charger configurations are designed and developed to realize improved power quality performance at the supply side and strictly comply with set national/international standards while operating under defined operating conditions. Each charger configuration's operational analysis, design, and control are analyzed comprehensively, considering wide operating conditions. Further, the overall performance of the proposed LEV

chargers is validated through software simulation and hardware implementation, and the obtained results are discussed in detail. Notably, the design, control, and overall performance objectives of the proposed unidirectional LEV chargers are validated under various steady state and dynamic operating conditions. Likewise, the bidirectional LEV chargers' performance is analyzed under G2V, V2G, and V2H mode conditions during normal/abnormal grid conditions and grid disconnection/reconnection events. Finally, the AC and DC side performance of the proposed unidirectional and bidirectional chargers are matched with set national/international standards to justify their compliance as high-performance LEV charging systems.

## सार

यह कार्य हल्के इलेक्ट्रिक वाहनों (एलईवी), यानी इलेक्ट्रिक दोपहिया वाहनों (ई2डब्ल्यू) और इलेक्ट्रिक थ्री व्हीलर (ई3डब्ल्यू) के लिए उच्च प्रदर्शन चार्जर के डिजाइन और विकास से संबंधित है। उपभोक्ताओं, निर्माताओं और बिजली आपूर्तिकर्ताओं के दृष्टिकोण से एलईवी चार्जर की कई वांछनीय प्रदर्शन विशेषताओं की पहचान की गई है और तदनुसार, इस कार्य में नए एलईवी चार्जर को डिजाइन, विश्लेषण और कार्यान्वित किया गया है। इस कार्य में बिजली प्रवाह की दिशा (यूनिडायरेक्शनल या द्विदिश), बिजली रूपांतरण चरणों की संख्या (एकल या डबल चरण), और अलगाव की आवश्यकता (गैर-पृथक या पृथक) के आधार पर एलईवी चार्जर का एक व्यापक वर्गीकरण किया गया है। विशेष रूप से, एलईवी के विभिन्न वर्गों के लिए एक सामान्य उद्देश्य/एकल चार्जिंग समाधान सुनिश्चित करने के लिए सभी चार्जर टोपोलॉजी को डिजाइन और कार्यान्वित करते समय आपूर्ति और बैटरी वोल्टेज स्थितियों की एक विस्तृत श्रृंखला पर विचार किया जाता है। इस कार्य में, ट्रांसफार्मर के पेशेवरों और विपक्षों का व्यापक रूप से विश्लेषण किया जाता है, और तदनुसार, एलईवी अनुप्रयोगों के लिए अलग-अलग उपन्यास नॉनसोलेटेड चार्जिंग समाधान प्रस्तावित किए जाते हैं। प्रस्तावित नॉनसोलेटेड एलईवी चार्जिंग समाधानों में, व्यापक एसी और डीसी साइड ऑपरेटिंग स्थितियों के तहत वांछित प्रदर्शन उद्देश्यों को प्राप्त करने के लिए ट्रांसफार्मर रहित लाभ समायोजन तकनीकों की प्रयोज्यता का व्यापक विश्लेषण किया जाता है। इसके अलावा, इन चार्जर टोपोलॉजी में फ़िल्टर आकार पर इनपुट-आउटपुट वर्तमान तरंगों के प्रभाव का पता लगाया जाता है, और इस कार्य में निरंतर इनपुट-आउटपुट वर्तमान विशेषताओं और कम फ़िल्टर आकार वाले कुछ नए LEV चार्जर प्रस्तावित किए गए हैं।

इसके अलावा, इस कार्य में एलईवी के लिए द्विदिशात्मक चार्जिंग प्रणाली की व्यवहार्यता का व्यापक मूल्यांकन किया गया है। तदनुसार, एलईवी उपभोक्ताओं और बिजली के लिए अधिक लाभ सुनिश्चित करने के लिए ग्रिड-टू-व्हीकल (जी2वी), व्हीकल-टू-ग्रिड (वी2जी), और व्हीकल-टू-होम (वी2एच) मोड परिचालन क्षमताओं के साथ विभिन्न नवीन द्विदिश एलईवी चार्जर प्रस्तावित हैं। आपूर्तिकर्ता। इसके अलावा, ग्रिड डिस्कनेक्शन और रीकनेक्शन घटनाओं के तहत प्रस्तावित द्विदिश एलईवी चार्जर्स की निर्बाध मोड ट्रांसफर क्षमता का गंभीर रूप से विश्लेषण किया जाता है, और तदनुसार, सामान्य/असामान्य परिचालन स्थितियों के तहत वांछित प्रदर्शन विशेषताओं को प्राप्त करने के लिए एक सरल लेकिन मजबूत नियंत्रण ढांचा तैयार किया जाता है।

विशेष रूप से, सभी प्रस्तावित यूनिडायरेक्शनल और बाइडायरेक्शनल चार्जर कॉन्फिगरेशन को आपूर्ति पक्ष में बेहतर बिजली गुणवत्ता प्रदर्शन का एहसास करने और परिभाषित परिचालन स्थितियों के तहत संचालन करते समय निर्धारित राष्ट्रीय/अंतर्राष्ट्रीय मानकों का सख्ती से अनुपालन करने के लिए डिज़ाइन और विकसित किया गया है। व्यापक परिचालन स्थितियों पर विचार करते हुए, प्रत्येक चार्जर कॉन्फिगरेशन के परिचालन विश्लेषण, डिज़ाइन और नियंत्रण का व्यापक विश्लेषण किया जाता है। इसके अलावा, प्रस्तावित एलईवी चार्जर्स के समग्र प्रदर्शन को सॉफ्टवेयर सिमुलेशन और हार्डवेयर कार्यान्वयन के माध्यम से मान्य किया गया है, और प्राप्त परिणामों पर विस्तार से चर्चा की गई है। विशेष रूप से, प्रस्तावित यूनिडायरेक्शनल एलईवी चार्जर्स के डिज़ाइन, नियंत्रण और समग्र प्रदर्शन उद्देश्यों को विभिन्न स्थिर स्थिति और गतिशील परिचालन स्थितियों के तहत मान्य किया गया है। इसी तरह, सामान्य/असामान्य ग्रिड स्थितियों और ग्रिड डिस्कनेक्शन/रीकनेक्शन घटनाओं के दौरान जी2वी, वी2जी और वी2एच मोड स्थितियों के तहत द्विदिश एलईवी चार्जर्स के प्रदर्शन का विश्लेषण किया जाता है। अंत में, प्रस्तावित यूनिडायरेक्शनल और बाइडायरेक्शनल चार्जर्स के एसी और डीसी साइड प्रदर्शन को उच्च-प्रदर्शन वाले एलईवी चार्जिंग सिस्टम के रूप में उनके अनुपालन को उचित ठहराने के लिए निर्धारित राष्ट्रीय/अंतर्राष्ट्रीय मानकों के साथ मिलान किया जाता है।

## TABLE OF CONTENTS

	<b>Page No.</b>
Certificate	i
Acknowledgement	ii
Abstract	iv
Table of Contents	viii
List of Figures	xx
List of Tables	xlii
List of Abbreviations	xliv
List of Symbols	xlvii
<b>CHAPTER I INTRODUCTION</b>	
1.1 General	1
1.2 State of Art of Electric Vehicle Technology	2
1.2.1 Review of Charging Levels and Standards	2
1.2.2 Classification of Battery Chargers	3
1.3 Existing LEV Chargers and Limitations	4
1.4 Objectives and Scope of Work	6
1.5 Chapter Outlines	8
<b>CHAPTER II LITERATURE SURVEY</b>	
2.1 General	11
2.2 Overview of Light Electric Vehicle’s Ecosystems	11
2.3 Literature Survey	13
2.3.1 Review of Unidirectional Electric Vehicle Chargers	14
2.3.2 Review of Bidirectional Electric Vehicle Chargers	17
2.4 Identified Research Area	20
2.5 Conclusions	21
<b>CHAPTER III UNIDIRECTIONAL SINGLE STAGE NONISOLATED LIGHT ELECTRIC VEHICLE CHARGERS</b>	
3.1 General	23
3.2 Configurations of Unidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	23
3.2.1 Bridgeless Switched Inductor Cuk PFC AC-DC Converter Based LEVs Charger	24
3.2.2 Bridgeless Switched Inductor SEPIC PFC AC-DC Converter Based LEVs Charger	24
3.3 Operating Principle of Unidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	25
3.3.1 Operating Principle and Steady State Analysis of BSIC PFC AC-DC Converter Based LEVs Charger	25
3.3.2 Operating Principle and Steady State Analysis of BSISEPIC PFC AC-DC Converter Based LEVs Charger	29

3.4	Design Guidelines and Component Selection of Unidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	33
3.4.1	Design Guidelines and Component Selection of BSIC PFC AC-DC Converter Based LEVs Charger	34
3.4.2	Design Guidelines and Component Selection of BSISEPIC PFC AC-DC Converter Based LEVs Charger	35
3.5	Control of Unidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	36
3.6	Software Modelling and Simulation of Unidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	37
3.7	Hardware Implementation of Unidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	38
3.8	Results and Discussion	39
3.8.1	Performance Validation of BSIC PFC AC-DC Converter Based LEVs Charger	39
3.8.1.1	Performance Analysis under Steady State Condition	39
3.8.1.2	Performance Analysis under Supply Voltage Dynamics	41
3.8.1.3	Performance Analysis under Load Dynamics	42
3.8.1.4	Improved Power Quality Performance at AC Mains	43
3.8.1.5	Performance Analysis during Starting Condition	45
3.8.2	Performance Validation of BSISEPIC PFC AC-DC Converter Based LEVs Charger	45
3.8.2.1	Performance Analysis under Steady State Condition	45
3.8.2.2	Performance Analysis under Supply Voltage Dynamics	47
3.8.2.3	Performance Analysis under Load Dynamics	48
3.8.2.4	Improved Power Quality Performance at AC Mains	49
3.8.2.5	Performance Analysis under Starting Condition	51
3.9	Comparative Analysis of Unidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	51
3.10	Conclusions	53
<b>CHAPTER IV UNIDIRECTIONAL SINGLE STAGE ISOLATED LIGHT ELECTRIC VEHICLE CHARGERS</b>		
4.1	General	54
4.2	Configurations of Unidirectional Single Stage Isolated Light Electric Vehicle Chargers	54
4.2.1	Fully Bridgeless Positive Output Buck-Boost (FBLPOBB) PFC AC-DC Converter Based LEVs Charger	55
4.2.2	Bridgeless Positive Output Luo (BLPOL) PFC AC-DC Converter Based LEVs Charger	56
4.2.3	Fully Bridgeless Positive Output Luo (FBLPOL) PFC AC-DC Converter Based LEVs Charger	56

4.2.4	Bridgeless SEPIC (BLSEPIC) PFC AC-DC Converter Based LEV Charger	57
4.2.5	Bridgeless Positive Output Cuk (BLPOC) PFC AC-DC Converter Based LEV Charger	58
4.2.6	Bridgeless Modified SEPIC (BLMSEPIC) PFC AC-DC Converter Based LEV Charger	58
4.3	Operating Principle of Unidirectional Single Stage Isolated Light Electric Vehicle Chargers	59
4.3.1	Operating Principle and Steady State Analysis of FBLPOBB PFC AC-DC Converter Based LEVs Charger	60
4.3.2	Operating Principle and Steady State Analysis of BLPOL PFC AC-DC Converter Based LEVs Charger	63
4.3.3	Operating Principle and Steady State Analysis of FBLPOL PFC AC-DC Converter Based LEVs Charger	67
4.3.4	Operating Principle and Steady State Analysis of BLSEPIC PFC AC-DC Converter Based LEVs Charger	69
4.3.5	Operating Principle and Steady State Analysis of BLPOC PFC AC-DC Converter Based LEVs Charger	73
4.3.6	Operating Principle and Steady State Analysis of BLMSEPIC PFC AC-DC Converter Based LEVs Charger	76
4.4	Design and component Selection of Unidirectional Single Stage Isolated Light Electric Vehicle Chargers	80
4.4.1	Design and Component Selection of FBLPOBB PFC AC-DC Converter Based LEVs Charger	80
4.4.2	Design and Component Selection of BLPOL PFC AC-DC Converter Based LEV Charger	82
4.4.3	Design and Component Selection of FBLPOL PFC AC-DC Converter Based LEV Charger	83
4.4.4	Design and Component Selection of BLSEPIC PFC AC-DC Converter Based LEV Charger	84
4.4.5	Design and Component Selection of BLPOC PFC AC-DC Converter Based LEV Charger	86
4.4.6	Design and Component Selection of BLMSEPIC PFC AC-DC Converter Based LEV Charger	88
4.5	Control of Unidirectional Single Stage Isolated Light Electric Vehicle Chargers	89
4.6	Software Simulations of Unidirectional Single Stage Isolated Light Electric Vehicle Chargers	90
4.7	Hardware Implementation of Unidirectional Single Stage Isolated Light Electric Vehicle Chargers	91
4.8	Results and Discussion	91
4.8.1	Performance of FBLPOBB PFC AC-DC Converter Based LEVs Charger	91
4.8.1.1	Performance Analysis under Steady State Condition	92

4.8.1.2	Performance Analysis under Supply Voltage Dynamics	93
4.8.1.3	Performance Analysis under Load Dynamics	94
4.8.1.4	Improved Power Quality Performance at AC Mains	95
4.8.1.5	Performance Analysis under Starting and Stopping Condition	97
4.8.2	Performance Validation of BLPOL PFC AC-DC Converter Based LEVs Charger	97
4.8.2.1	Performance Analysis under Steady State Condition	97
4.8.2.2	Performance Analysis under Supply Voltage Dynamics	99
4.8.2.3	Improved Power Quality Performance at AC Mains	100
4.8.3	Performance Validation of FBLPOL PFC AC-DC Converter Based LEVs Charger	101
4.8.3.1	Performance Analysis under Steady State Condition	101
4.8.3.2	Performance Analysis under Supply Voltage Dynamics	103
4.8.3.3	Performance Analysis under Load Dynamics	105
4.8.3.4	Improved Power Quality Performance at AC Mains	105
4.8.3.5	Performance Analysis under Starting and Stopping Condition	106
4.8.4	Performance of BLSEPIC PFC AC-DC Converter Based LEV Charger	107
4.8.4.1	Performance Analysis under Steady State Condition	107
4.8.4.2	Performance Analysis under Supply Voltage Dynamics	109
4.8.4.3	Performance Analysis under Load Dynamics	109
4.8.4.4	Improved Power Quality Performance at AC Mains	110
4.8.4.5	Performance Analysis under Starting Condition	112
4.8.5	Performance of BLPOC PFC AC-DC Converter Based LEV Charger	112
4.8.5.1	Performance Analysis under Steady State Condition	112
4.8.5.2	Performance Analysis under Supply Voltage Dynamics	114
4.8.5.3	Performance Analysis under Load Dynamics	115
4.8.5.4	Improved Power Quality Performance at AC Mains	116
4.8.5.5	Performance Analysis under Starting and Stopping Condition	116
4.8.6	Performance of BLMSEPIC PFC AC-DC Converter Based LEV Charger	117
4.8.6.1	Performance Analysis under Steady State Condition	117
4.8.6.2	Performance Analysis under Supply Voltage Dynamics	119

4.8.6.3	Performance Analysis under Load Dynamics	119
4.8.6.4	Improved Power Quality Performance at AC Mains	120
4.8.6.5	Performance Analysis under Starting and Stopping Condition	122
4.9	Comparative Analysis of Unidirectional Single Stage Isolated Light Electric Vehicle Chargers	122
4.10	Conclusions	126
<b>CHAPTER V UNIDIRECTIONAL DOUBLE STAGE NONISOLATED LIGHT ELECTRIC VEHICLE CHARGERS</b>		
5.1	General	127
5.2	Configurations of Unidirectional Double Stage Non-Isolated Light Electric Vehicle Chargers	127
5.2.1	Partially Bridgeless CSC (PBLCSC) PFC AC-DC Stage and High Gain Buck (HGB) DC-DC Stage Based Double Stage Non-Isolated LEVs Charger	128
5.2.2	Fully Bridgeless CSC (FBLCSC) PFC AC-DC Stage and High Gain Buck (HGB) DC-DC Stage Based Double Stage Nonisolated LEVs Charger	128
5.3	Operating Principle of Unidirectional Double Stage Non-Isolated Light Electric Vehicle Chargers	129
5.3.1	Operating Principle and Steady State Analysis of PBLCSC PFC AC-DC Stage and HGB DC-DC Stage Based Double Stage Non-Isolated LEVs Charger	130
5.3.1.1	Operating Principle and Steady State Analysis of PBLCSC PFC AC-DC Stage	130
5.3.1.2	Operating Principle and Steady State Analysis of HGB DC-DC Stage	133
5.3.2	Operating Principle and Steady State Analysis of FBLCSC PFC AC-DC Stage and HGB DC-DC Stage Based Double Stage Non-Isolated LEVs Charger	135
5.3.2.1	Operating Principle and Steady State Analysis of FBLCSC PFC AC-DC Stage	135
5.3.2.2	Operating Principle and Steady State Analysis of HGB DC-DC Stage	140
5.4	Design Guidelines and Component Selection of Unidirectional Double Stage Nonisolated Light Electric Vehicle Chargers	140
5.4.1	Design Guidelines and Component Selection of PBLCSC and FBLCSC PFC AC-DC Converters	140
5.4.2	Design Guidelines and Component Selection of HGB DC-DC Stage	142
5.5	Control of Unidirectional Double Stage Nonisolated Light Electric Vehicle Chargers	142

5.5.1	Control of PBL CSC PFC AC-DC Stage and HGB DC-DC Stage Based Double Stage Non-Isolated LEVs Charger	143
5.5.1.1	Control of PBL CSC PFC AC-DC Stage	143
5.5.1.2	Control of HGB DC-DC Stage	144
5.5.2	Control of FBL CSC PFC AC-DC Stage and HGB DC-DC Stage Based Double Stage Non-Isolated LEVs Charger	145
5.5.2.1	Control of FBL CSC PFC AC-DC Stage	145
5.5.2.2	Control of HGB DC-DC Stage	146
5.6	Software Modelling and Simulation of Unidirectional Double Stage Nonisolated Light Electric Vehicle Chargers	147
5.7	Hardware Implementation of Unidirectional Double Stage Nonisolated Light Electric Vehicle Chargers	147
5.8	Results and Discussion	148
5.8.1	Performance Validation PBL CSC PFC AC-DC Stage and HGB DC-DC Stage Based Double Stage Nonisolated LEVs Charger	149
5.8.1.1	Performance Analysis under Steady State Condition	149
5.8.1.2	Performance Analysis under Supply Voltage Dynamics	151
5.8.1.3	Performance Analysis under Load Dynamics	152
5.8.1.4	Improved Power Quality Performance at AC Mains	153
5.8.2	Performance Validation of FBL CSC PFC AC-DC Stage and HGB DC-DC Stage Based Double Stage Nonisolated LEVs Charger	154
5.8.2.1	Performance Analysis under Steady State Condition	155
5.8.2.2	Performance Analysis under Supply Voltage Dynamics	157
5.8.2.3	Performance Analysis under Load Dynamics	158
5.8.2.4	Performance Analysis under Variable DC Link Voltage	159
5.8.2.5	Improved Power Quality Performance at AC Mains	160
5.9	Comparative Analysis of Unidirectional Double Stage Nonisolated Light Electric Vehicle Chargers	161
5.10	Conclusions	163
<b>CHAPTER VI UNIDIRECTIONAL DOUBLE STAGE ISOLATED LIGHT ELECTRIC VEHICLE CHARGERS</b>		
6.1	General	165
6.2	Configurations of Unidirectional Double Stage Isolated Light Electric Vehicle Chargers	165
6.2.1	IL CSC PFC AC-DC Stage and IPOC DC-DC Stage Based LEV Charger	166
6.2.2	MSC CSC PFC AC-DC Stage and IPOC DC-DC Stage Based LEV Charger	166
6.3	Operating Principle of Unidirectional Double Stage Isolated Light Electric Vehicle Chargers	167

6.3.1	Operating Principle and Steady State Analysis of ILCSC PFC AC-DC Stage and IPOC DC-DC Stage Based LEVs Charger	168
6.3.1.1	Operating Principle and Steady State Analysis of ILCSC PFC Stage	168
6.3.1.2	Operating Principle and Steady State Analysis of IPOC DC-DC Stage	172
6.3.2	Operating Principle and Steady State Analysis of MSCCSC PFC AC-DC Stage and IPOC DC-DC Stage Based LEVs Charger	174
6.3.2.1	Derivation, Operation, and Steady State Analysis of MSCCSC PFC Stage	174
6.3.2.2	Operation and Steady State Analysis of IPOC DC-DC Stage	178
6.4	Design Guidelines and Component Selection of Unidirectional Double Stage Isolated Light Electric Vehicle Chargers	178
6.4.1	Design and Component Selection Guidelines of ILCSC PFC AC-DC Converter and IPOC DC-DC Converter Based LEVs Charger	179
6.4.1.1	Design of ILCSC PFC AC-DC Converter	179
6.4.1.2	Design of IPOC DC-DC Converter	180
6.4.2	Design Guidelines and Component Selection of MSCCSC PFC AC-DC Converter and IPOC DC-DC Converter Based LEVs Charger	183
6.4.2.1	Design of MSCCSC PFC AC-DC Converter	183
6.4.2.2	Design of IPOC DC-DC Converter	185
6.5	Control of Unidirectional Double Stage Isolated Light Electric Vehicle Chargers	185
6.5.1	Control of ILCSC PFC AC-DC Stage and IPOC DC-DC Stage-Based Charger	185
6.5.1.1	Control of ILCSC PFC AC-DC Converter	185
6.5.1.2	Control of IPOC DC-DC Converter	186
6.5.2	Control of MSCCSC PFC AC-DC Stage and IPOC DC-DC Stage-Based Charger	187
6.5.2.1	Control of MSCCSC PFC AC-DC Stage	187
6.5.2.2	Control of IPOC DC-DC Stage	188
6.6	Software Simulations of Unidirectional Double Stage Isolated Light Electric Vehicle Chargers	188
6.7	Hardware Implementation of Unidirectional Double Stage Isolated Light Electric Vehicle Chargers	189
6.8	Results and Discussion	189
6.8.1	Performance Validation of ILCSC PFC AC-DC Stage and IPOC DC-DC Stage Based LEVs Charger	189
6.8.1.1	Performance Analysis under Steady State Condition	189
6.8.1.2	Performance Analysis under Supply Voltage Dynamics	192

6.8.1.3	Performance Analysis under Load Dynamics	193
6.8.1.4	Improved Power Quality Performance at AC Mains	194
6.8.2	Performance Validation of MSCCSC PFC AC-DC Stage and IPOC DC-DC Stage Based LEVs Charger	195
6.8.2.1	Performance Analysis under Steady State Condition	195
6.8.2.2	Performance Validation of Wide Operating Range Feature of MSCCSC PFC AC-DC Stage	197
6.8.2.3	Performance Analysis under Supply Voltage Dynamics	198
6.8.2.4	Performance Analysis under Load Dynamics	199
6.8.2.5	Improved Power Quality Performance at AC Mains	200
6.9	Comparative Analysis of Unidirectional Double Stage Isolated Light Electric Vehicle Chargers	201
6.10	Conclusions	203
<b>CHAPTER VII BIDIRECTIONAL SINGLE STAGE NONISOLATED LIGHT ELECTRIC VEHICLE CHARGERS</b>		
7.1	General	205
7.2	Configurations of Bidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	205
7.2.1	Active Switched Inductor Cuk (ASIC) Converter Based Bidirectional Single-Stage Charger	206
7.2.2	Active Switched Inductor SEPIC (ASISEPIC) Converter Based Bidirectional Single Stage Charger	206
7.3	Operating Principle of Bidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	207
7.3.1	Operating Principle and Steady State Analysis of ASIC Converter Based Bidirectional LEVs Charger	208
7.3.2	Operating Principle and Steady State Analysis of ASISEPIC Converter Based Bidirectional LEVs Charger	213
7.4	Design Guidelines and Component Selection of Bidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	218
7.5	Control of Bidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	219
7.6	Software Simulations of Bidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	221
7.7	Hardware Implementation of Bidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	222
7.8	Results and Discussion	222
7.8.1	Performance Validation of ASIC Converter Based Bidirectional LEVs Charger	223
7.8.1.1	Performance Analysis under G2V Mode Operation	223
7.8.1.1.1	Performance Analysis during Steady State	223

	7.8.1.1.2	Performance Analysis during Supply Voltage and Load Dynamics	225
	7.8.1.1.3	Improved Power Quality Performance under G2V Mode	226
	7.8.1.2	Performance Analysis under V2G Mode Operation	227
	7.8.1.2.1	Performance Analysis during Steady State	227
	7.8.1.2.2	Performance Analysis during Supply Voltage and Load Dynamics	229
	7.8.1.2.3	Improved Power Quality Performance under V2G Mode	231
7.8.2		Performance Validation of ASISEPIC Converter Based Bidirectional LEV Charger	231
	7.8.2.1	Performance Analysis under G2V Mode Operation	232
	7.8.2.1.1	Performance Analysis during Steady State	232
	7.8.2.2.2	Performance Analysis during Supply Voltage and Load Dynamics	233
	7.8.2.2.3	Improved Power Quality Performance	234
	7.8.2.2	Performance Analysis under V2G Mode Operation	235
	7.8.2.2.1	Performance Analysis during Steady State	236
	7.8.2.2.2	Performance Analysis during Supply Voltage and Load Dynamics	238
	7.8.2.2.3	Improved Power Quality Performance	239
7.9		Comparative Analysis of Bidirectional Single Stage Nonisolated Light Electric Vehicle Chargers	240
7.10		Conclusions	241
<b>CHAPTER VIII BIDIRECTIONAL SINGLE STAGE ISOLATED LIGHT ELECTRIC VEHICLE CHARGERS</b>			
8.1		General	243
8.2		Configurations of Bidirectional Single Stage Isolated Light Electric Vehicle Chargers	243
	8.2.1	Fully Bridgeless Bidirectional SEPIC (FBLBSEPIC) based LEV Charger	244
	8.2.2	Fully Bridgeless Bidirectional Luo (FBLBL) Converter based LEV Charger	244
8.3		Operating Principle of Bidirectional Single Stage Isolated Light Electric Vehicle Chargers	245
	8.3.1	Operating Principle and Steady State Analysis of FBLBSEPIC Converter Based Bidirectional LEV Charger	245
	8.3.2	Operating Principle and Steady State Analysis of FBLBL Converter Based Bidirectional LEV Charger	251

8.4	Design and Component Selection of Bidirectional Single Stage Isolated Light Electric Vehicle Chargers	256
8.5	Control of Bidirectional Single Stage Isolated Light Electric Vehicle Chargers	258
8.6	Software Simulations of Bidirectional Single Stage Isolated Light Electric Vehicle Chargers	259
8.7	Hardware Implementation of Bidirectional Single Stage Isolated Light Electric Vehicle Chargers	260
8.8	Results and Discussion	260
8.8.1	Performance Analysis of FBLBSEPIC Converter Based Bidirectional LEVs Charger	261
8.8.1.1	Performance Analysis during G2V Mode Operation	261
8.8.1.1.1	Performance under Steady State Condition	261
8.8.1.1.2	Performance under Supply Voltage and Battery Current Dynamics	263
8.8.1.1.3	Improved Power Quality Performance	264
8.8.1.2	Performance Analysis during V2G/V2H Mode Operation	265
8.8.1.2.1	Performance under Steady State Condition	265
8.8.1.2.2	Performance under Supply Voltage and Battery Current Dynamics	267
8.8.1.2.3	Improved Power Quality Performance	269
8.8.2	Performance Analysis of FBLBL Converter Based Bidirectional LEVs Charger	270
8.8.2.1	Performance Analysis during G2V Mode Operation	270
8.8.2.1.1	Performance under Steady State Condition	270
8.8.2.1.2	Performance under Supply Voltage and Battery Current Dynamics	272
8.8.2.1.3	Improved Power Quality Performance	273
8.8.2.2	Performance Analysis during V2G/V2H Mode Operation	274
8.8.2.2.1	Performance under Steady State Condition	274
8.8.2.2.2	Performance under Supply Voltage and Battery Current Dynamics	276
8.8.2.2.3	Improved Power Quality Performance Analysis	278
8.9	Comparative Analysis of Bidirectional Single Stage Isolated Light Electric Vehicle Chargers	278
8.10	Conclusions	280

<b>CHAPTER IX</b>		<b>BIDIRECTIONAL DOUBLE STAGE NON-ISOLATED LIGHT ELECTRIC VEHICLE CHARGER</b>	
9.1	General		281
9.2	Configuration Of Bidirectional Double Stage Non-Isolated Light Electric Vehicle Charger		281
9.3	Operating Principle of Bidirectional Double Stage Non-Isolated Light Electric Vehicle Charger		282
9.4	Design and Component Selection of Bidirectional Double Stage Non-Isolated Light Electric Vehicle Charger		287
9.5	Control Of Bidirectional Double Stage Non-Isolated Light Electric Vehicle Charger		289
9.5.1	Control of Front-End AC-DC Stage		289
	9.5.1.1 Control during G2V/V2G Mode Operation		289
	9.5.1.2 Control during V2H and Seamless Mode Transfer Conditions		293
9.5.2	Control of Back End DC-DC Stage		293
	9.5.2.1 Control during G2V/V2G Mode Operation		294
	9.5.2.2 Control during V2H Mode Operation		294
9.6	Performance Validation of Bidirectional Double Stage Non-Isolated Light Electric Vehicle Charger		295
9.7	Results and Discussion		296
9.7.1	Performance Analysis under Grid Connected Mode Operation (G2V/V2G)		296
	9.7.1.1 Performance Analysis under Steady State Condition		297
	9.7.1.2 Performance under Supply Voltage Dynamics		302
	9.7.1.3 Performance under Charging Current Dynamics		303
	9.7.1.4 Performance of Charger under Distorted Grid Condition		303
	9.7.1.5 Performance of Charger under Grid Frequency Variations		304
	9.7.1.6 Performance under G2V-V2G and V2G-G2V Mode Transition		305
	9.7.2 Performance under Grid Disconnected Mode Operation (V2H)		306
	9.7.3 Performance during Grid Disconnection and Reconnection Mode		307
9.8	Conclusions		308
<b>CHAPTER X</b>		<b>BIDIRECTIONAL DOUBLE STAGE ISOLATED LIGHT ELECTRIC VEHICLE CHARGER</b>	
10.1	General		310
10.2	Configuration Of Bidirectional Double Stage Isolated Light Electric Vehicle Charger		310
10.3	Operating Principle of Bidirectional Double Stage Isolated Light Electric Vehicle Charger		311

10.4	Design and Component Selection of Bidirectional Double Stage Isolated Light Electric Vehicle Charger	316
10.5	Control of Bidirectional Double Stage Isolated Light Electric Vehicle Charger	318
10.5.1	Control of Front-End AC-DC Stage	319
10.5.1.1	Control during G2V/V2G Mode Operation	319
10.5.1.2	Control during V2H and Seamless Mode Transfer Conditions	320
10.5.2	Control of Back End DC-DC Stage	321
10.6	Performance Validation of Bidirectional Double Stage Isolated Light Electric Vehicle Charger	322
10.7	Results and Discussion	323
10.7.1	Performance under Grid Connected Mode Operation (G2V/V2G)	323
10.7.1.1	Performance Analysis under Steady State Condition	323
10.7.1.2	Performance under Supply Voltage Dynamics	327
10.7.1.3	Performance under Change in Active and Reactive Power Demand at Grid	327
10.7.1.4	Power Quality Performance of Charger under Distorted Grid Condition	329
10.7.1.5	Performance Under G2V-V2G and V2G-G2V Mode Transfer	330
10.7.2	Performance under Grid Disconnected Mode Operation (V2H)	331
10.7.3	Performance during Grid Disconnection and Reconnection Mode	332
10.8	Conclusions	333
<b>CHAPTER XI MAIN CONCLUSIONS AND SUGGESTIONS FOR FURTHER WORK</b>		
11.1	General	334
11.2	Main Conclusions	335
11.3	Suggestions for Further Work	339
<b>REFERENCES</b>		341
<b>APPENDICES</b>		362
<b>LIST OF PUBLICATIONS</b>		372
<b>BIO DATA</b>		376

## LIST OF FIGURES

- Fig. 1.1 AC Connector Interface Options for 1- $\phi$  AC Slow Charging (a) BEVs without OBCs (b) BEVs with OBCs (c) BEVs with OBCs and Cable attached to EVSE.
- Fig. 3.1 BSIC PFC AC-DC Converter based Unidirectional Single Stage Non isolated LEV Charger.
- Fig. 3.2 BSISEPIC AC-DC Converter based Unidirectional Single Stage Nonisolated LEV Charger.
- Fig. 3.3 Operating Modes of BSIC PFC AC-DC Converter Based LEVs Charger within a Switching Cycle (during Positive Half of  $v_s$ ) (a) Mode-P(I) ( $t_0 < t \leq t_1$ ) (b) Mode-P(II) ( $t_1 < t \leq t_2$ ) (c) Mode-P(III) ( $t_2 < t \leq t_3$ ).
- Fig. 3.4 Switching Cycle Voltage and Current Waveforms for BSIC PFC AC-DC Converter Based LEVs Charger (during Positive Half of  $v_s$ )
- Fig. 3.5 Operating Modes of BSIC PFC AC-DC Converter based LEV Charger within a Switching Cycle (during Negative Half of  $v_s$ ) (a) Mode-N(I) ( $t_0 < t \leq t_1$ ) (b) Mode-N(II) ( $t_1 < t \leq t_2$ ) (c) Mode-N(III) ( $t_2 < t \leq t_3$ ).
- Fig. 3.6 Operation of BSISEPIC PFC based LEV Charger in Positive Cycle of  $v_s$  (a) *Mode-P(I)* ( $t_0 < t \leq t_1$ ) (b) *Mode-P(II)* ( $t_1 < t \leq t_2$ ) (c) *Mode-P(III)* ( $t_2 < t \leq t_3$ ).
- Fig. 3.7 Switching Cycle Voltage and Current Waveforms for BSISEPIC PFC AC-DC Converter Based LEVs Charger (during Positive Half of  $v_s$ )
- Fig. 3.8 Operation of BSISEPIC PFC AC-DC Converter based LEV Charger in Negative Cycle of  $v_s$  (a) *Mode-P(I)* ( $t_0 < t \leq t_1$ ) (b) *Mode-P(II)* ( $t_1 < t \leq t_2$ ) (c) *Mode-P(III)* ( $t_2 < t \leq t_3$ )
- Fig. 3.9 Control Block Diagram for Unidirectional Single Stage Nonisolated Chargers.
- Fig. 3.10 General Block Diagram for Software Modelling and MATLAB Simulation of Unidirectional Single Stage Nonisolated LEV Chargers.
- Fig. 3.11 Test Bench Set-up for Unidirectional Single Stage Nonisolated LEV Chargers.
- Fig. 3.12 Simulated Performance of BSIC PFC AC-DC Converter based LEV Charger Under Steady State Nominal Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{C1}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (b)  $v_s$ ,  $v_{S1}$ ,  $v_{S2}$ ,  $i_{S1}$ ,  $v_{Ds1}$ ,  $v_{Ds2}$ , and  $i_{Ds1}$ .
- Fig. 3.13 Experimental performance of BSIC PFC AC-DC converter based LEV charger under steady state nominal operating condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ , and  $i_{bat}$  (b)  $v_s$ ,  $v_{C1}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (c)  $v_{S1}$ ,  $v_{S2}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (d)  $v_{Ds1}$ ,  $v_{Ds2}$ , and  $i_{Ls1}$ .
- Fig. 3.14 Simulated performance of BSIC PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V to 160 V and (b) 220 V to 265 V.
- Fig. 3.15 Experimental performance of BSIC PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V to 160 V and (b) 220 V to 265 V.
- Fig. 3.16 Simulated performance of BSIC PFC AC-DC converter based LEV charger under charging current dynamics from (a) Rated to Half of Rated, and (b) Half of Rated to Rated Conditions.

- Fig. 3.17 Experimental performance of BSIC PFC AC-DC converter based LEV charger under charging current dynamics (a) Rated to Half of Rated, and (b) Half of Rated to Rated Conditions.
- Fig. 3.18 Simulated supply side power quality performance of BSIC PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a) 220 V, (b) 160 V, and (c) 265 V
- Fig. 3.19 Experimental validation of supply side power quality performance of BSIC PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a)-(c) 220 V (d)-(f) 170 V, and (g)-(i) 250 V.
- Fig. 3.20 Experimental validation of supply side power quality performance of BSIC PFC AC-DC converter based LEV charger at low power condition and supply voltage of (a)-(c) 220 V (d)-(f) 85 V, and (g)-(i) 260 V.
- Fig. 3.21 Experimental performance of BSIC PFC AC-DC converter based LEV during start of battery charging process at rated power condition.
- Fig. 3.22 Simulated Performance of BSISEPIC PFC AC-DC Converter based LEV Charger Under Steady State Nominal Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{C1}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (b)  $v_s$ ,  $v_{S1}$ ,  $v_{S2}$ ,  $i_{S1}$ ,  $v_{Ds1}$ ,  $v_{Ds2}$ , and  $i_{Ds1}$ .
- Fig. 3.23 Experimental performance of BSISEPIC PFC AC-DC converter based LEV charger under steady state nominal operating condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ , and  $i_{bat}$  (b)  $v_s$ ,  $v_{C1}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (c)  $v_{S1}$ ,  $v_{S2}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (d)  $v_{Ds1}$ ,  $v_{Ds2}$ , and  $i_{Ls1}$ .
- Fig. 3.24 Simulated performance of BSISEPIC PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V to 265 V, and (b) 220 V to 160 V.
- Fig. 3.25 Experimental performance of BSISEPIC PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub>.
- Fig. 3.26 Simulated performance of BSISEPIC PFC AC-DC converter based LEV charger under charging current dynamics (a) Rated to Half of Rated, and (b) Half of Rated to Rated Conditions.
- Fig. 3.27 Experimental performance of BSISEPIC PFC AC-DC converter based LEV charger under charging current dynamics (a) Rated to Half of Rated, and (b) Half of Rated to Rated Conditions.
- Fig. 3.28 Simulated supply side power quality performance of BSISEPIC PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a) 220 V, (b) 160 V, and (c) 265 V.
- Fig. 3.29 Experimental validation of supply side power quality performance of BSISEPIC PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a)-(c) 220 V (d)-(f) 160 V, and (g)-(i) 250 V.
- Fig. 3.30 Experimental validation of supply side power quality performance of BSISEPIC PFC AC-DC converter based LEV charger at low power conditions and supply voltage of (a)-(c) 220 V (d)-(f) 85 V, and (g)-(i) 250 V.

- Fig. 3.31 Experimental performance of BSISEPIC PFC AC-DC converter based LEV during start of battery charging process at rated power condition.
- Fig. 3.32 Power Vs Efficiency Curve for BSIC and BSISEPIC PFC AC-DC Converter Based Charger at Rated Supply Voltage Condition.
- Fig. 4.1 FBLPOBB PFC AC-DC Converter based unidirectional single stage isolated LEV Charger.
- Fig. 4.2 BLPOL PFC AC-DC converter based unidirectional single stage isolated LEV charger.
- Fig. 4.3 FBLPOL PFC AC-DC Converter based Unidirectional Single Stage Isolated LEV Charger
- Fig. 4.4. BLSEPIC PFC AC-DC Converter based Unidirectional Single Stage Isolated LEV Charger.
- Fig. 4.5. BLPOC PFC AC-DC Converter based Unidirectional Single Stage Isolated LEV Charger.
- Fig. 4.6. BLMSEPIC PFC AC-DC Converter based Unidirectional Single Stage Isolated LEV Charger.
- Fig. 4.7. Equivalent Circuit of FBLPOBB PFC AC-DC Converter based LEV Charger during (a) Positive and (b) Negative Half Cycle of  $v_s$ .
- Fig. 4.8. Operating Modes of FBLPOBB PFC AC-DC Converter Based LEVs Charger within a Switching Cycle (during Positive Half of  $v_s$ ) (a) *Mode-P(I)* ( $t_0 < t \leq t_1$ ) (b) *Mode-P(II)* ( $t_1 < t \leq t_2$ ) (c) *Mode-P(III)* ( $t_2 < t \leq t_3$ )
- Fig. 4.9. Switching Cycle Voltage/Current Waveforms of FBLPOBB PFC AC-DC Converter Based LEV Charger during Positive Half of  $v_s$ .
- Fig. 4.10. Equivalent Circuit of BLPOL PFC AC-DC Converter based LEV Charger during (a) Positive and (b) Negative Half Cycle of  $v_s$ .
- Fig. 4.11. Operating Modes of BLPOL PFC AC-DC Converter Based LEVs Charger within a Switching Cycle (during Positive Half of  $v_s$ ) (a) *Mode-P(I)* ( $t_0 < t \leq t_1$ ) (b) *Mode-P(II)* ( $t_1 < t \leq t_2$ ) (c) *Mode-P(III)* ( $t_2 < t \leq t_3$ ).
- Fig. 4.12. Switching Cycle Voltage/Current Waveforms of BLPOL PFC AC-DC Converter Based LEV Charger during Positive Half of  $v_s$ .
- Fig. 4.13. Equivalent Circuits of FBLPOL PFC AC-DC Converter based LEV Charger during (a) Positive and (b) Negative Half Cycle of  $v_s$ .
- Fig. 4.14. Operating Modes of FBLPOL PFC AC-DC Converter Based LEVs Charger within a Switching Cycle (during Positive Half of  $v_s$ ) (a) *Mode-P(I)* ( $t_0 < t \leq t_1$ ) (b) *Mode-P(II)* ( $t_1 < t \leq t_2$ ) (c) *Mode-P(III)* ( $t_2 < t \leq t_3$ ).
- Fig. 4.15. Switching Cycle Voltage/Current Waveforms of FBLPOL PFC AC-DC Converter Based LEV Charger during Positive Half of  $v_s$ .
- Fig. 4.16. Equivalent Circuit of BLSPEIC PFC AC-DC Converter based LEV Charger during (a) Positive and (b) Negative Half Cycle of  $v_s$ .

- Fig. 4.17. Operating Modes of BLSEPIC PFC AC-DC Converter Based LEVs Charger within a Switching Cycle (during Positive Half of  $v_s$ ) (a) *Mode-P(I)* ( $t_0 < t \leq t_1$ ) (b) *Mode-P(II)* ( $t_1 < t \leq t_2$ ) (c) *Mode-P(III)* ( $t_2 < t \leq t_3$ ).
- Fig. 4.18. Switching Cycle Voltage/Current Waveforms of BLSEPIC PFC AC-DC Converter Based LEV Charger during Positive Half of  $v_s$ .
- Fig. 4.19. Equivalent Circuit of BLPOC PFC AC-DC Converter based LEV Charger during (a) Positive and (b) Negative Half Cycle of  $v_s$ .
- Fig. 4.20. Operating Modes of BLPOC PFC AC-DC Converter Based LEVs Charger within a Switching Cycle (during Positive Half of  $v_s$ ) (a) *Mode-P(I)* ( $t_0 < t \leq t_1$ ) (b) *Mode-P(II)* ( $t_1 < t \leq t_2$ ) (c) *Mode-P(III)* ( $t_2 < t \leq t_3$ ).
- Fig. 4.21. Switching Cycle Voltage/Current Waveforms of BLPOC PFC AC-DC Converter Based LEV Charger during Positive Half of  $v_s$ .
- Fig. 4.22. Equivalent Circuit of BLMSEPIC PFC AC-DC Converter based LEV Charger during (a) Positive and (b) Negative Half Cycle of  $v_s$ .
- Fig. 4.23. Operating Modes of BLMSEPIC PFC AC-DC Converter Based LEVs Charger within a Switching Cycle (during Positive Half of  $v_s$ ) (a) *Mode-P(I)* ( $t_0 < t \leq t_1$ ) (b) *Mode-P(II)* ( $t_1 < t \leq t_2$ ) (c) *Mode-P(III)* ( $t_2 < t \leq t_3$ ).
- Fig. 4.24. Switching Cycle Voltage/Current Waveforms of BLMSEPIC PFC AC-DC Converter Based LEV Charger during Positive Half of  $v_s$ .
- Fig. 4.25. Control Block Diagram for Unidirectional Single Stage Isolated LEV Chargers.
- Fig. 4.26. General Block Diagram for Software Modelling and MATLAB Simulation of Unidirectional Single Stage Isolated LEV Chargers.
- Fig. 4.27. Test Bench Set-up for Unidirectional Single Stage Isolated LEV Chargers.
- Fig. 4.28. Simulated Performance of FBLPOBB PFC AC-DC Converter based LEV Charger Under Steady State Nominal Operating Condition (a)  $v_s, i_s, v_{bat}, i_{bat}, v_{Cf1}, v_{Cf2}, i_{pri1}$ , and  $i_{sec1}$  (b)  $v_s, v_{S1}, i_{S1}, v_{S2}, i_{S2}, v_{Do1}, i_{Do1}, v_{Do2}$ , and  $i_{Do2}$ .
- Fig. 4.29. Experimental performance of FBLPOBB PFC AC-DC converter based LEV charger under steady state nominal operating condition (a)  $v_s, i_s, v_{bat}$ , and  $i_{bat}$  (b)  $v_s, v_{Cf2}$ , and  $v_{Cf1}$  (c)  $v_s, v_{S1}, v_{S2}$ , and  $i_{S1}$  (d)  $v_s, v_{Do1}, v_{Do2}$ , and  $i_{Do1}$ .
- Fig. 4.30. Simulated performance of FBLPOBB PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V to 85 V and (b) 220 V to 265 V.
- Fig. 4.31. Experimental performance of FBLPOBB PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V<sub>RMS</sub> to 85 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>.
- Fig. 4.32. Simulated performance of FBLPOBB PFC AC-DC converter based LEV charger under charging current dynamics from (a) 100% to 50%, and (b) 50% to 100% Rated Conditions.
- Fig. 4.33. Experimental performance of FBLPOBB PFC AC-DC converter based LEV charger under charging current dynamics (a) 100% to 50%, and (b) 50% to 100% of Rated Conditions.

- Fig.4.34. Simulated supply side power quality performance of FBLPOBB PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a) 220 V, (b) 265 V, and (c) 85 V.
- Fig.4.35. Experimental validation of supply side power quality performance of FBLPOBB PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a)-(c) 220 V (d)-(f) 250 V, and (g)-(i) 95 V.
- Fig. 4.36. Experimental validation of supply side power quality performance of FBLPOBB PFC AC-DC converter based LEV charger at low power conditions and supply voltage of (a)-(c) 220 V (d)-(f) 250 V, and (g)-(i) 85 V.
- Fig. 4.37. Experimental performance of FBLPOBB PFC AC-DC converter based LEV during (a) Starting and (b) Stopping battery charging process at rated power condition.
- Fig. 4.38. Simulated Performance of BLPOL PFC AC-DC Converter based LEV Charger Under Steady State Nominal Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{C1}$ ,  $i_{Lo}$ , and  $i_{sec}$  (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{S2}$ ,  $i_{S2}$ ,  $v_{Do}$ , and  $i_{Do}$ .
- Fig. 4.39. Experimental performance of BLPOL PFC AC-DC converter based LEV charger under steady state nominal operating condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ , and  $i_{bat}$  (b)  $v_s$ ,  $v_{C1}$ ,  $i_{Lo}$ , and  $i_{Do}$  (c)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ , and  $i_{Do}$  (d)  $v_s$ ,  $v_{S2}$ ,  $v_{S1}$ , and  $v_{Do}$ , (e)  $v_{S1}$ ,  $v_{S2}$ ,  $v_{Db1}$ , and  $v_{Db2}$ .
- Fig. 4.40. Simulated performance of BLPOL PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V<sub>RMS</sub> to 85 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>.
- Fig. 4.41. Experimental performance of BLPOL PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V<sub>RMS</sub> to 85V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>.
- Fig.4.42. Simulated supply side power quality performance of BLPOL PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a) 220 V, (b) 265 V, and (c) 85 V.
- Fig.4.43. Experimental validation of supply side power quality performance of BLPOL PFC AC-DC converter-based LEV charger at rated power condition and supply voltage of (a)-(c) 220 V (d)-(f) 265 V, and (g)-(i) 85 V.
- Fig. 4.44. Simulated Performance of FBLPOL PFC AC-DC Converter based LEV Charger Under Steady State Nominal Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{Cf1}$ ,  $v_{cf2}$ ,  $v_{C1}$ , and  $i_{Lo}$  (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{S2}$ ,  $i_{S2}$ ,  $v_{Do1}$ ,  $i_{Do1}$ ,  $v_{Do2}$ , and  $i_{Do2}$ .
- Fig. 4.45. Experimental performance of FBLPOL PFC AC-DC converter based LEV charger under steady state nominal operating condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ , and  $i_{bat}$  (b)  $v_s$ ,  $v_{Cf1}$ ,  $v_{C1}$ , and  $i_{Lo}$  (c)  $v_s$ ,  $v_{Cf1}$ , and  $v_{Cf2}$  (c)  $v_s$ ,  $v_{S2}$ ,  $v_{S1}$ , and  $i_{S1}$  (d)  $v_s$ ,  $v_{Do1}$ ,  $v_{Do2}$ , and  $i_{Do1}$ .
- Fig. 4.46. Simulated performance of FBLPOL PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V<sub>RMS</sub> to 85 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>.

- Fig. 4.47. Experimental performance of FBLPOL PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V<sub>RMS</sub> to 85 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>.
- Fig. 4.48. Simulated performance of FBLPOL PFC AC-DC converter based LEV charger under charging current dynamics from (a) 100% to 50% and (b) 50% to 100% of Rated Condition.
- Fig. 4.49. Experimental performance of FBLPOL PFC AC-DC converter based LEV charger under charging current dynamics (a) 100% to 50%, and (b) 50% to 100% of Rated Conditions.
- Fig.4.50. Simulated supply side power quality performance of FBLPOL PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a) 220 V, (b) 265 V, and (c) 85 V.
- Fig.4.51. Experimental validation of supply side power quality performance of FBLPOL PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a)-(c) 220 V (d)-(f) 250 V, and (g)-(i) 95 V.
- Fig. 4.52. Experimental validation of supply side power quality performance of FBLPOL PFC AC-DC converter based LEV charger at low power conditions and supply voltage of (a)-(c) 220 V (d)-(f) 250 V, and (g)-(i) 85 V.
- Fig. 4.53. Experimental performance of FBLPOL PFC AC-DC converter based LEV during (a) Starting and (b) Stopping battery charging process at rated power condition.
- Fig. 4.54. Simulated Performance of BLSEPIC PFC AC-DC Converter based LEV Charger Under Steady State Nominal Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $i_{pri}$ ,  $v_{C1}$ ,  $v_{C2}$ ,  $i_{Li1}$ , and  $i_{Li2}$  (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{D1}$ ,  $v_{D2}$ ,  $v_{Do}$ ,  $i_{Do}$ ,  $v_{Db1}$  and  $v_{Db2}$ .
- Fig. 4.55. Experimental performance of BLSPEIC PFC AC-DC converter based LEV charger under steady state nominal operating condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ , and  $i_{bat}$  (b)  $v_{C1}$ ,  $v_{C2}$ ,  $i_{Li2}$ , and  $i_{Li1}$  (c)  $v_s$ ,  $v_{D2}$ , and  $v_{D1}$  (d)  $v_{S1}$ ,  $i_{pri}$ ,  $v_{Do}$ , and  $i_{sec}$ .
- Fig. 4.56. Simulated performance of BLSEPIC PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V to 160 V and (b) 220 V to 265 V.
- Fig. 4.57. Experimental performance of BLSEPIC PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V<sub>RMS</sub> to 150 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>.
- Fig. 4.58. Simulated performance of BLSEPIC PFC AC-DC converter based LEV charger under charging current dynamics from (a) 100% to 50% and (b) 50% to 100% of Rated Condition.
- Fig. 4.59. Experimental performance of BLSEPIC PFC AC-DC converter based LEV charger during charging current dynamics (a) 100% to 50%, and (b) 50% to 100% of Rated Condition.
- Fig.4.60. Simulated supply side power quality performance of BLSEPIC PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a) 220 V, (b) 265 V, and (c) 160 V.

- Fig.4.61. Experimental validation of supply side power quality performance of BLSEPIC PFC AC-DC converter-based LEV charger at rated power condition and supply voltage of (a)-(c) 220 V (d)-(f) 260 V, and (g)-(i) 150 V.
- Fig.4.62. Experimental validation of supply side power quality performance of BLSEPIC PFC AC-DC converter-based LEV charger at low power conditions and supply voltage of (a)-(c) 220 V (d)-(f) 265 V, and (g)-(i) 85 V.
- Fig. 4.63. Experimental performance of BLSEPIC PFC AC-DC converter-based LEV during Starting of battery charging process at rated power condition.
- Fig. 4.64. Simulated Performance of BLPOC PFC AC-DC Converter based LEV Charger Under Steady State Nominal Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{C1}$ ,  $v_{C2}$ , and  $i_{Lo}$  (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{S2}$ ,  $i_{S2}$ ,  $v_{Do}$ , and  $i_{Do}$ .
- Fig. 4.65. Experimental performance of BLPOC PFC AC-DC converter-based LEV charger under steady state nominal operating condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ , and  $i_{bat}$  (b)  $v_s$ ,  $v_{C1}$ ,  $v_{C2}$ , and  $i_{Lo}$  (c)  $v_{S1}$ ,  $v_{S2}$ ,  $v_{Do}$ , and  $i_{Lo}$  (d)  $v_s$ ,  $v_{S2}$ ,  $v_{S1}$ , and  $v_{Do}$ .
- Fig. 4.66. Simulated performance of BLPOC PFC AC-DC converter-based LEV charger under supply voltage dynamics from (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>.
- Fig. 4.67. Experimental performance of BLPOC PFC AC-DC converter-based LEV charger under supply voltage dynamics from (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>.
- Fig. 4.68. Simulated performance of BLPOC PFC AC-DC converter-based LEV charger under charging current dynamics from (a) 100% to 50% and (b) 50% to 100% of Rated Conditions.
- Fig. 4.69. Experimental performance of BLPOC PFC AC-DC converter-based LEV charger under charging current dynamics (a) 100% to 50%, and (b) 50% to 100% of Rated Conditions.
- Fig.4.70. Simulated supply side power quality performance of BLPOL PFC AC-DC converter-based LEV charger at rated power condition and supply voltage of (a) 220 V, (b) 265 V, and (c) 160 V.
- Fig.4.71. Experimental validation of supply side power quality performance of BLPOC PFC AC-DC converter-based LEV charger at rated power condition and supply voltage of (a)-(c) 220 V (d)-(f) 250 V, and (g)-(i) 160 V.
- Fig.4.72. Experimental validation of supply side power quality performance of BLPOC PFC AC-DC converter-based LEV charger at low power conditions and supply voltage of (a)-(c) 220 V (d)-(f) 250 V, and (g)-(i) 85 V.
- Fig. 4.73. Experimental performance of BLPOC PFC AC-DC converter-based LEV during (a) Starting and (b) Stopping battery charging process at rated power condition.
- Fig. 4.74. Simulated Performance of BLMSPEIC PFC AC-DC Converter based LEV Charger Under Steady State Nominal Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{C1}$ ,  $v_{Cs1}$ ,  $v_{Cs2}$ ,  $i_{Lo}$ , and  $i_{sec}$ , (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{S2}$ ,  $i_{S2}$ ,  $v_{Ds1}$ ,  $i_{Ds1}$ ,  $v_{Ds2}$ , and  $i_{Ds2}$ .

- Fig. 4.75. Experimental performance of BLMSPEIC PFC AC-DC converter-based LEV charger under steady state nominal operating condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ , and  $i_{bat}$  (b)  $v_{C1}$ ,  $v_{Cs1}$ ,  $v_{Cs2}$ , and  $i_{Lo}$  (c)  $v_{Ds1}$ ,  $v_{Ds2}$ ,  $i_{pri}$ , and  $i_{sec}$ , (d)  $v_s$ ,  $v_{S1}$ ,  $v_{S2}$ , and  $v_{Ds1}$ .
- Fig. 4.76. Simulated performance of BLMSEPIC PFC AC-DC converter-based LEV charger under supply voltage dynamics from (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>.
- Fig. 4.77. Experimental performance of BLMSEPIC PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>.
- Fig. 4.78. Simulated performance of BLMSEPIC PFC AC-DC converter based LEV charger under charging current dynamics from (a) 100% to 50% and (b) 50% to 100% of Rated Conditions.
- Fig. 4.79. Experimental performance of BLMSPEIC PFC AC-DC converter-based LEV charger during charging current dynamics (a) 100% to 50%, and (b) 50% to 100% of Rated Condition.
- Fig.4.80. Simulated supply side power quality performance of BLMSEPIC PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a) 220 V, (b) 265 V, and (c) 160 V.
- Fig.4.81. Experimental validation of supply side power quality performance of BLMSEPIC PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a)-(c) 220 V (d)-(f) 250 V, and (g)-(i) 160 V.
- Fig.4.82. Experimental validation of supply side power quality performance of BLMSEPIC PFC AC-DC converter based LEV charger at low power conditions and supply voltage of (a)-(c) 220 V (d)-(f) 260 V, and (g)-(i) 90 V.
- Fig. 4.83. Experimental performance of BLMSEPIC PFC AC-DC converter based LEV Charger during (a) Starting and (b) Stopping battery charging process at rated power condition.
- Fig. 4.84. Efficiency Versus Battery Current Graph for (a) FBLPOBB, (b) BLPOL, (c) FBLPOL, (d) BLSEPIC, (e) BLPOC, and (f) BLMSEPIC PFC AC-DC converter based LEV Chargers.
- Fig. 5.1. PBLCSC PFC Converter based Unidirectional Double Stage Non-isolated LEV Charger.
- Fig. 5.2. FBLCSC PFC Converter based Unidirectional Double Stage Nonisolated LEV Charger.
- Fig. 5.3. Equivalent Circuit of PBLCSC PFC AC-DC Converter based LEV Charger during (a) Positive and (b) Negative Half Cycle of  $v_s$ .
- Fig. 5.4. Operating Modes of PBLCSC PFC AC-DC Converter Based LEVs Charger within a Switching Cycle (during Positive Half of  $v_s$ ) (a) *Mode-P(I)*  $\{0 < t \leq D_s T_s\}$  (b) *Mode-P(II)*  $\{D_s T_s < t \leq (D_s + D_D) T_s\}$  (c) *Mode-P(III)*  $\{(D_s + D_D) T_s < t \leq T_s\}$

- Fig. 5.5. Switching Cycle Voltage/Current Waveforms of PBLCSC PFC AC-DC Converter Based LEV Charger during (a) Positive and (b) Negative Half of  $v_s$ .
- Fig. 5.6. Operating Modes of PBLCSC PFC AC-DC Converter Based LEVs Charger within a Switching Cycle (Negative Half of  $v_s$ ) (a) *Mode-N(I)*  $\{0 < t \leq D_s T_s\}$  (b) *Mode-N(II)*  $\{D_s T_s < t \leq (D_s + D_D) T_s\}$  (c) *Mode-N(III)*  $\{(D_s + D_D) T_s < t \leq T_s\}$ .
- Fig. 5.7. (a)-(b) Operating Modes of HGB DC-DC Stage within a Switching Cycle (a) *Mode-1*  $\{0 < t \leq D_b T_s\}$  (b) *Mode-2*  $\{D_b T_s < t \leq T_s\}$  and (c) Switching Cycle Voltage/Current Waveforms.
- Fig. 5.8. Equivalent Circuit of FBLCSC PFC AC-DC Converter based LEV Charger during (a) Positive and (b) Negative Half Cycle of  $v_s$ .
- Fig. 5.9. Operating Modes of FBLCSC PFC AC-DC Converter Based LEVs Charger within a Switching Cycle (during Positive Half of  $v_s$ ) (a) *Mode-P(I)*  $\{0 < t \leq D_s T_s\}$  (b) *Mode-P(II)*  $\{D_s T_s < t \leq (D_s + D_D) T_s\}$  (c) *Mode-P(III)*  $\{(D_s + D_D) T_s < t \leq T_s\}$ .
- Fig. 5.10. Operating Modes of FBLCSC PFC AC-DC Converter Based LEVs Charger within a Switching Cycle (during Negative Half of  $v_s$ ) (a) *Mode-N(I)*  $\{0 < t \leq D_s T_s\}$  (b) *Mode-N(II)*  $\{D_s T_s < t \leq (D_s + D_D) T_s\}$  (c) *Mode-N(III)*  $\{(D_s + D_D) T_s < t \leq T_s\}$ .
- Fig. 5.11. Switching Cycle Voltage/Current Waveforms of FBLCSC PFC AC-DC Converter Based LEV Charger during (a) Positive and (b) Negative Half of  $v_s$ .
- Fig. 5.12. Control Block Diagram for PBLCSC PFC AC-DC Stage of Unidirectional Double Stage Non-isolated LEV Charger.
- Fig. 5.13. Control Block Diagram for HGB DC-DC Stage of Unidirectional Double Stage Nonisolated LEV Charger.
- Fig. 5.14. Variation of HGB Switch Duty Ratio at Different  $V_{bat}$  with and without  $V_{DC}$  Variations.
- Fig. 5.15. Control Block Diagram for FBLCSC PFC AC-DC Stage of Unidirectional Double Stage Nonisolated LEV Charger.
- Fig. 5.16. General Block Diagram for Software Modelling and MATLAB Simulation of Unidirectional Double Stage Non-isolated LEV Chargers.
- Fig. 5.17. Test Bench Photograph for Unidirectional Double Stage Nonisolated LEV Chargers.
- Fig. 5.18. Simulated Performance of PBLCSC PFC AC-DC Converter based LEV Charger Under Steady State Nominal Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{DC}$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{C1}$ ,  $v_{C2}$ ,  $i_{Li1}$ ,  $i_{Li2}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (b)  $v_s$ ,  $v_{S1}$ ,  $v_{S2}$ ,  $i_{S1}$ ,  $v_{D1}$ ,  $v_{D2}$ ,  $i_{D1}$ ,  $v_{S3}$ ,  $v_{Ds1}$ , and  $v_{Ds2}$ .
- Fig. 5.19. Experimental performance of PBLCSC PFC AC-DC converter based LEV charger under steady state nominal operating condition (a)  $v_s$ ,  $i_s$ ,  $v_{DC}$ , and  $i_{bat}$  (b)  $v_s$ ,  $i_s$ ,  $v_{bat}$ , and  $i_{bat}$  (c)  $v_s$ ,  $v_{S1}$ ,  $v_{D1}$ , and  $i_{Li1}$  (d)  $v_s$ ,  $v_{S2}$ ,  $v_{D2}$ , and  $i_{Li2}$  (e)  $v_s$ ,  $v_{C1}$ ,  $v_{C2}$ , and  $v_{DC}$  (f)  $v_{S2}$ ,  $v_{S1}$ ,  $v_{D1}$ , and  $v_{D2}$  (g)  $v_{S3}$ ,  $v_{Ds1}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (h)  $v_{DC}$ ,  $v_{S3}$ ,  $v_{Ds1}$ , and  $v_{Ds2}$ .
- Fig. 5.20. Simulated performance of PBLCSC PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220  $V_{RMS}$  to 160  $V_{RMS}$  and (b) 220  $V_{RMS}$  to 265  $V_{RMS}$ .

- Fig. 5.21. Experimental performance of PBLCS C PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220  $V_{RMS}$  to 160  $V_{RMS}$  and (b) 220  $V_{RMS}$  to 265  $V_{RMS}$ .
- Fig. 5.22. Simulated performance of PBLCS C PFC AC-DC converter based LEV charger under charging current dynamics from (a) 100 % to 50%, and (b) 50 % to 100 % Conditions.
- Fig. 5.23. Experimental performance of PBLCS C PFC AC-DC converter-based LEV charger under charging current dynamics (a) Rated to Half of Rated, and (b) Half of Rated to Rated Conditions.
- Fig. 5.24. Simulated supply side power quality performance of PBLCS C PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a) 220 V, (b) 160 V, and (c) 265 V.
- Fig. 5.25. Experimental validation of supply side power quality performance of PBLCS C PFC AC-DC converter based LEV charger at  $P_{rated}$  and  $v_s$  of (a)-(c) 220 V (d)-(f) 160 V, and (g)-(i) 255 V.
- Fig. 5.26. Experimental validation of supply side power quality performance of PBLCS C PFC based LEV charger at low power condition and  $v_s$  of (a)-(c) 220 V (d)-(f) 250 V, and (g)-(i) 110 V.
- Fig. 5.27. Simulated Performance of FBLCS C PFC AC-DC Converter based LEV Charger Under Steady State Nominal Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{DC}$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{Cf1}$ ,  $v_{Cf2}$ ,  $v_{C1}$ ,  $v_{C2}$ ,  $i_{Li1}$ ,  $i_{Li2}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{S2}$ ,  $i_{S2}$ ,  $v_{D1}$ ,  $i_{D1}$ ,  $v_{D2}$ ,  $i_{D2}$ ,  $v_{S3}$ ,  $i_{S3}$ ,  $v_{Ds1}$ , and  $v_{Ds2}$ .
- Fig. 5.28. Experimental performance of FBLCS C PFC AC-DC converter based LEV charger under steady state nominal operating condition (a)  $v_s$ ,  $i_s$ ,  $v_{DC}$ , and  $i_{bat}$  (b)  $v_s$ ,  $i_s$ ,  $v_{bat}$ , and  $i_{bat}$  (c)  $v_s$ ,  $v_{S1}$ ,  $v_{D1}$ , and  $i_{Li1}$  (d)  $v_s$ ,  $v_{S2}$ ,  $v_{D2}$ , and  $i_{Li2}$  (e)  $v_{S1}$ ,  $v_{D1}$ ,  $v_{S2}$ , and  $v_{D2}$  (f)  $v_{Cf1}$ ,  $v_{C2}$ ,  $v_{Cf2}$ , and  $v_{C1}$  (g)  $v_{DC}$ ,  $v_{S3}$ ,  $v_{Ds1}$ , and  $v_{Ds2}$  (h)  $v_{S3}$ ,  $v_{Ds1}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$ .
- Fig. 5.29. Simulated performance of FBLCS C PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220  $V_{RMS}$  to 160  $V_{RMS}$  and (b) 220  $V_{RMS}$  to 265  $V_{RMS}$ .
- Fig. 5.30. Experimental performance of FBLCS C PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220  $V_{RMS}$  to 160  $V_{RMS}$  and (b) 220  $V_{RMS}$  to 265  $V_{RMS}$ .
- Fig. 5.31. Simulated performance of FBLCS C PFC AC-DC converter based LEV charger under charging current dynamics from (a) 100 % to 50%, and (b) 50 % to 100 % Conditions.
- Fig. 5.32. Experimental performance of FBLCS C PFC AC-DC converter based LEV charger under charging current dynamics (a) Rated to Half of Rated, and (b) Half of Rated to Rated Conditions.
- Fig. 5.33. Variable DC Link Voltage Control of FBLCS C PFC AC-DC converter based LEV charger.

- Fig. 5.34. Simulated supply side power quality performance of FBLCSC PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a) 220 V, (b) 160 V, and (c) 265 V.
- Fig. 5.35. Experimental validation of supply side power quality performance of FBLCSC PFC AC-DC converter based LEV charger at  $P_{rated}$  and  $v_s$  of (a)-(c) 220 V (d)-(f) 160 V, and (g)-(i) 250 V.
- Fig. 5.36. Experimental validation of supply side power quality performance of FBLCSC PFC-based LEV charger at low power conditions and  $v_s$  of (a)-(c) 220 V (d)-(f) 250 V, and (g)-(i) 110 V.
- Fig. 5.37. Efficiency Versus Power Graph for PBLCSC and FBLCSC PFC AC-DC Stages under Wide  $v_s$  and Power Range Condition (@  $V_{DC} = 300$  V).
- Fig. 5.38. Efficiency Versus Power Graph for HGB DC-DC Stage and PBLCSC/FBLCSC PFC Based Charger at Rated Operating Conditions (i.e.,  $V_{DC} = 300$  V,  $V_{batn} = 60$  V,  $V_s = 220$  V).
- Fig. 6.1 ILCSC PFC AC-DC Converter based Unidirectional Double Stage Isolated LEV Charger.
- Fig. 6.2 MSCCSC PFC AC-DC Converter based Unidirectional Double Stage Isolated LEV Charger.
- Fig. 6.3. ILCSC PFC AC-DC Converter Switching Devices Operating States within a Switching Cycle during (a) Overlapped (b) Non-overlapped Inductor Current Conditions.
- Fig. 6.4. Switching Equivalent Circuits of ILCSC PFC AC-DC Stage under Overlapped Inductor Current Condition during (a) State-I (b) State-II (c) State-III (d) State-IV (e) State-V (f) State-VI.
- Fig. 6.5. Switching Equivalent Circuits of ILCSC PFC AC-DC Stage under Non-Overlapped Inductor Current Condition during (a) State-I (b) State-II (c) State-III (d) State-IV (e) State-V (f) State-VI.
- Fig. 6.6. Waveforms across ILCSC PFC Converter's Components under all Six Switching Modes for Inductor Current (a) Overlapping (b) Non-overlapping Conditions.
- Fig. 6.7. (a)-(b) Operating Modes of IPOC DC-DC Stage within a Switching Cycle (a) *Mode-1*  $\{0 < t \leq D_b T_s\}$  (b) *Mode-2*  $\{D_b T_s < t \leq T_s\}$  and (c) Switching Cycle Voltage/Current Waveforms.
- Fig. 6.8. Circuit Schematic of (a) Conventional CSC [40], (b) Modified CSC, and (c) Proposed MSCCSC PFC AC-DC Converters.
- Fig. 6.9. Switching Cycle Equivalent Circuits of MSCCSC PFC AC-DC Converter (a) State-I, (b) State-II, (c) State-III, and (d) Switching Cycle Voltage and Current Waveforms
- Fig. 6.10. Voltage Gain of Conventional CSC [40] and MSCCSC PFC AC-DC Converters.
- Fig. 6.11. Control Block Diagram for ILCSC PFC AC-DC Stage of Unidirectional Double Stage Isolated LEV Charger.

- Fig. 6.12. Control Block Diagram for IPOC DC-DC Stage of Unidirectional Double Stage Isolated LEV Charger.
- Fig. 6.13. Control Block Diagram for MSCCSC PFC AC-DC Stage of Unidirectional Double Stage Isolated LEV Charger.
- Fig. 6.14. General Block Diagram for Software Modelling and MATLAB Simulation of Unidirectional Double Stage Isolated LEV Chargers.
- Fig. 6.15. Simulated Performance of ILCSC PFC AC-DC Converter based LEV Charger Under Steady State Nominal Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{DC}$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{C1}$ ,  $v_{C2}$ ,  $i_{Li1}$ ,  $i_{Li2}$ ,  $v_{S1}$ ,  $v_{S2}$ ,  $v_{D1}$ , and  $v_{D2}$ , and (b)  $v_{DC}$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{C1c}$ ,  $v_{C2c}$ ,  $i_{Lic}$ ,  $i_{Loc}$ ,  $v_{Sc}$ ,  $i_{Sc}$ ,  $v_{Dc}$ , and  $i_{Dc}$ .
- Fig. 6.16. Experimental performance of ILCSC PFC AC-DC converter based LEV charger under steady state nominal operating condition (a)  $v_s$ ,  $i_s$ ,  $v_{DC}$ , and  $i_{bat}$  (b)  $v_{C1}$ ,  $v_{C2}$ ,  $i_{Li1}$ , and  $i_{Li2}$  (c)  $v_{S1}$ ,  $v_{S2}$ ,  $i_{Li1}$ , and  $i_{Li2}$  (d)  $v_{S2}$ ,  $v_{S1}$ ,  $v_{D1}$ , and  $v_{D2}$  (e)  $v_{Sc}$ ,  $v_{Dc}$ ,  $i_{Lic}$ , and  $i_{Loc}$ , and (f)  $v_{DC}$ ,  $v_{C1c}$ ,  $v_{C2c}$ , and  $v_{bat}$ .
- Fig. 6.17. Simulated performance of ILCSC PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V to 160 V and (b) 220 V to 265 V.
- Fig. 6.18. Experimental performance of ILCSC PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V to 160 V and (b) 220 V to 265 V<sub>RMS</sub>.
- Fig. 6.19. Simulated performance of ILCSC PFC AC-DC converter based LEV charger under charging current dynamics from (a) 100 % to 50%, and (b) 50 % to 100 % Conditions.
- Fig. 6.20. Experimental performance of ILCSC PFC AC-DC converter-based LEV charger under-charging current dynamics (a) 100%-50%, and (b) 50 %-100 % Conditions.
- Fig. 6.21. Simulated supply side power quality performance of ILCSC PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a) 220 V, (b) 265 V, and (c) 160 V.
- Fig. 6.22. Experimental validation of supply side power quality performance of ILCSC PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a)-(c) 220 V (d)-(f) 265 V, and (g)-(i) 160 V.
- Fig. 6.23. Experimental validation of supply side power quality performance of ILCSC PFC AC-DC converter based LEV charger at low power conditions and supply voltage of (a)-(c) 220 V (d)-(f) 265 V, and (g)-(i) 95 V.
- Fig. 6.24. Simulated Performance of MSCCSC PFC AC-DC Converter based LEV Charger Under Steady State Nominal Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{DC}$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{C1}$ ,  $v_{Cs1}$ ,  $v_{Cs2}$ ,  $i_{Li}$ ,  $i_{Lo}$ ,  $v_{S1}$ ,  $v_{Ds1}$ , and  $v_{Ds2}$ , and (b)  $v_{DC}$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{C1c}$ ,  $v_{C2c}$ ,  $i_{Lic}$ ,  $i_{Loc}$ ,  $v_{Sc}$ ,  $i_{Sc}$ ,  $v_{Dc}$ , and  $i_{Dc}$ .
- Fig. 6.25. Experimental performance of MSCCSC PFC AC-DC converter based LEV charger under steady state nominal operating condition (a)  $v_s$ ,  $i_s$ ,  $v_{DC}$ , and  $i_{bat}$  (b)  $v_{C1}$ ,  $v_{Cs1}$ ,  $v_{Cs2}$ , and  $i_{Lo}$  (c)  $v_s$ ,  $v_{S1}$ ,  $v_{Ds1}$ , and  $i_{Li}$  (d)  $v_s$ ,  $v_{S1}$ ,  $v_{Ds1}$ , and  $v_{Ds2}$  (e)  $v_{DC}$ ,  $v_{C1c}$ ,  $v_{C2c}$ , and  $v_{bat}$ , and (f)  $v_{Sc}$ ,  $v_{Dc}$ ,  $i_{Lic}$ , and  $i_{Loc}$ .

- Fig. 6.26. Experimental performance of MSCCSC PFC AC-DC converter based LEV charger under Wide Operating Range Condition,  $V_s$ ,  $I_s$ , and  $V_{DC}$ , when (a)  $V_s = 85 V_{RMS}$  &  $V_{DC} = 400 V$ , (b)  $V_s = 85 V_{RMS}$  &  $V_{DC} = 200 V$ , (c)  $V_s = 265 V_{RMS}$  &  $V_{DC} = 400 V$ , and (d)  $V_s = 265 V_{RMS}$  &  $V_{DC} = 200 V$ .
- Fig. 6.27. Simulated performance of MSCCSC PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220 V to 160 V and (b) 220 V to 265 V.
- Fig. 6.28. Experimental performance of MSCCSC PFC AC-DC converter based LEV charger under supply voltage dynamics from (a) 220  $V_{RMS}$  to 160  $V_{RMS}$  and (b) 220  $V_{RMS}$  to 265  $V_{RMS}$ .
- Fig. 6.29. Simulated performance of MSCCSC PFC AC-DC converter based LEV charger under charging current dynamics from (a) 100 % to 50%, and (b) 50 % to 100 % Conditions.
- Fig. 6.30. Experimental performance of MSCCSC PFC AC-DC converter-based LEV charger under charging current dynamics (a) 100 % to 50%, and (b) 50 % to 100 % Conditions.
- Fig. 6.31. Simulated supply side power quality performance of MSCCSC PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a) 220 V, (b) 265 V, and (c) 160 V.
- Fig. 6.32. Experimental validation of supply side power quality performance of MSCCSC PFC AC-DC converter based LEV charger at rated power condition and supply voltage of (a)-(c) 220 V (d)-(f) 265 V, and (g)-(i) 165 V.
- Fig. 6.33. Experimental validation of supply side power quality performance of MSCCSC PFC AC-DC converter-based LEV charger at low power conditions and supply voltage of (a)-(c) 220 V (d)-(f) 250 V, and (g)-(i) 85 V.
- Fig. 6.34. Loss Analysis and Efficiency Analysis of (a) ILCSC PFC AC-DC Stage, (b) MSCCSC PFC AC-DC Stage, and (c) IPOC DC-DC Stage at Rated Operating Conditions.
- Fig. 7.1 ASIC Converter based Bidirectional Single Stage Nonisolated LEV Charger.
- Fig. 7.2. ASISEPIC Converter based Bidirectional Single Stage Nonisolated LEV Charger.
- Fig. 7.3. Operating Modes of ASIC Converter Based Bidirectional LEVs Charger during (a) G2V (b) V2G (for positive half of  $v_s$ ) and (c) V2G (for negative half of  $v_s$ ).
- Fig. 7.4. Switching Cycle Operating Modes of ASIC Converter Based Bidirectional LEVs Charger during G2V Mode Operation (a) Mode-G2V (I) ( $t_0 < t \leq t_1$ ) (b) Mode-G2V (II) ( $t_1 < t \leq t_2$ ) (c) Mode-G2V (III) ( $t_2 < t \leq t_3$ ).
- Fig. 7.5. Switching Cycle Operating Modes of ASIC Converter Based Bidirectional LEVs Charger during V2G Mode Operation (Positive Half of  $v_s$ ) (a) Mode-V2G (P<sub>1</sub>) ( $t_0 < t \leq t_1$ ) (b) Mode-V2G (P<sub>2</sub>) ( $t_1 < t \leq t_2$ ) (c) Mode-V2G (P<sub>3</sub>) ( $t_2 < t \leq t_3$ ).
- Fig. 7.6. Switching Cycle Voltage and Current Waveforms for ASIC Converter Based Bidirectional LEVs Charger during (a) G2V and (b) V2G (Positive Half of  $v_s$ ) Modes of Operation.

- Fig. 7.7. Operating Modes of ASISEPIC Converter Based Bidirectional LEVs Charger during (a) G2V (b) V2G (positive half of  $v_s$ ) and (c) V2G (for negative half of  $v_s$ ).
- Fig. 7.8. Switching Cycle Operating Modes of ASISEPIC Converter Based Bidirectional LEVs Charger during G2V Mode Operation (a) Mode-G2V (I) ( $t_0 < t \leq t_1$ ) (b) Mode-G2V (II) ( $t_1 < t \leq t_2$ ) (c) Mode-G2V (III) ( $t_2 < t \leq t_3$ ).
- Fig. 7.9. Switching Cycle Operating Modes of ASISEPIC Converter Based Bidirectional LEVs Charger during V2G Mode Operation (Positive Half of  $v_s$ ) (a) Mode-V2G (P<sub>1</sub>) ( $t_0 < t \leq t_1$ ) (b) Mode-V2G (P<sub>2</sub>) ( $t_1 < t \leq t_2$ ) (c) Mode-V2G (P<sub>3</sub>) ( $t_2 < t \leq t_3$ ).
- Fig. 7.10. Switching Cycle Voltage and Current Waveforms for ASISEPIC Converter Based Bidirectional LEVs Charger during (a) G2V and (b) V2G (Positive Half of  $v_s$ ) Modes of Operation.
- Fig. 7.11. Control Block Diagram for Bidirectional Single Stage Nonisolated LEV Chargers.
- Fig. 7.12. General Block Diagram for Software Modelling and MATLAB Simulation of Bidirectional Single Stage Nonisolated LEV Chargers.
- Fig. 7.13. Proof-of-Concept Test Bench Set-up for Bidirectional Single Stage Nonisolated LEV Chargers.
- Fig. 7.14. Simulated Steady State Performance of ASIC Converter-based Bidirectional LEV Charger during G2V Mode Operation (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $i_{Li}$ ,  $v_{C1}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{Ss1}$ ,  $v_{Ss2}$ ,  $i_{Ss1}$ ,  $v_{Sa1}$ ,  $i_{Sa1}$ ,  $v_{Sa2}$ ,  $i_{Sa2}$ ,  $v_{Sa3}$ , and  $v_{Sa4}$ .
- Fig. 7.15. Experimental Steady State performance of ASIC Converter based Bidirectional LEV charger during G2V Mode Operation (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ , and  $i_{bat}$  (b)  $v_s$ ,  $i_s$ ,  $i_{Li}$ , and  $v_{C1}$  (c)  $v_{Ss1}$ ,  $v_{Ss2}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (d)  $v_s$ ,  $v_{S1}$ ,  $v_{Ss1}$ , and  $v_{Ss2}$ .
- Fig. 7.16. Simulated performance of ASIC Converter based Bidirectional LEV charger during G2V Mode Operation under (a)-(b)  $v_s$  dynamics from (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub> and (c)-(d)  $i_{bat}$  dynamics from (c) 100% to 50%, and (d) 50% to 100% Conditions.
- Fig. 7.17. Experimental performance of ASIC Converter based Bidirectional LEV charger during G2V Mode Operation under (a)-(b)  $v_s$  dynamics from (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub> and (c)-(d)  $i_{bat}$  dynamics from (c) 100% to 50%, and (d) 50% to 100% Conditions.
- Fig. 7.18. Simulated supply side power quality performance of ASIC Converter based Bidirectional LEV charger during G2V Mode and supply voltage of (a) 220 V, (b) 160 V, and (c) 265 V.
- Fig. 7.19. Experimental validation of supply side power quality performance of ASIC Converter-based LEV charger during G2V and supply voltage of (a)-(c) 220 V (d)-(f) 160 V, and (g)-(i) 255 V.
- Fig. 7.20. Simulated Steady State Performance of ASIC Converter based Bidirectional LEV Charger during V2G Mode Operation (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $i_{Li}$ ,  $v_{C1}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{Ss1}$ ,  $v_{Ss2}$ ,  $i_{Ss1}$ ,  $v_{Sa1}$ ,  $i_{Sa1}$ ,  $v_{Sa2}$ ,  $i_{Sa2}$ ,  $v_{Sa3}$ , and  $v_{Sa4}$ .

- Fig. 7.21. Experimental Steady State performance of ASIC Converter based Bidirectional LEV charger during V2G Mode Operation (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ , and  $i_{bat}$  (b)  $v_s$ ,  $i_s$ ,  $i_{Li}$ , and  $v_{C1}$  (c)  $v_{Ss1}$ ,  $v_{Ss2}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (d)  $v_s$ ,  $v_{S1}$ ,  $v_{Ss1}$ , and  $v_{Ss2}$  (e)  $v_{Sa1}$ ,  $v_{Sa2}$ ,  $v_{Sa3}$ , and  $v_{Sa4}$ .
- Fig. 7.22. Simulated performance of ASIC Converter based Bidirectional LEV charger during V2G Mode Operation under (a)-(b)  $v_s$  dynamics from (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub> and (c)-(d)  $i_{bat}$  dynamics from (c) 100% to 50%, and (d) 50% to 100% Conditions.
- Fig. 7.23. Experimental performance of ASIC Converter based Bidirectional LEV charger during V2G Mode Operation under (a)-(b)  $v_s$  dynamics from (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub> and (c)-(d)  $i_{bat}$  dynamics from (c) 100% to 50%, and (d) 50% to 100% Conditions.
- Fig. 7.24. Simulated supply side power quality performance of ASIC Converter based Bidirectional LEV charger during V2G Mode and  $v_s$  of (a) 220 V, (b) 160 V, and (c) 265 V.
- Fig. 7.25. Experimental validation of supply side power quality performance of ASIC Converter-based LEV charger during V2G and  $v_s$  of (a)-(c) 220 V (d)-(f) 165 V, and (g)-(i) 255V.
- Fig. 7.26. Simulated Steady State Performance of ASISEPIC Converter-based Bidirectional LEV Charger during G2V Mode (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $i_{Li}$ ,  $v_{C1}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{Ss1}$ ,  $v_{Ss2}$ ,  $i_{Ss1}$ ,  $v_{Sa1}$ ,  $i_{Sa1}$ ,  $v_{Sa2}$ ,  $i_{Sa2}$ ,  $v_{Sa3}$ , and  $v_{Sa4}$ .
- Fig. 7.27. Experimental Steady State performance of ASISEPIC Converter based Bidirectional LEV charger during G2V Mode Operation (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ , and  $i_{bat}$  (b)  $v_s$ ,  $i_s$ ,  $i_{Li}$ , and  $v_{C1}$  (c)  $v_{Ss1}$ ,  $v_{Ss2}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (d)  $v_s$ ,  $v_{S1}$ ,  $v_{Ss1}$ , and  $v_{Ss2}$ .
- Fig. 7.28. Simulated performance of ASISEPIC Converter-based Bidirectional LEV charger during G2V Mode Operation under (a)-(b)  $v_s$  dynamics from (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub> and (c)-(d)  $i_{bat}$  dynamics from (c) 100% to 50%, and (d) 50% to 100% Conditions.
- Fig. 7.29. Experimental performance of ASISEPIC Converter-based Bidirectional LEV charger during G2V Mode Operation under (a)-(b)  $v_s$  dynamics from (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub> and (c)-(d)  $i_{bat}$  dynamics from (c) 100% to 50%, and (d) 50% to 100% Conditions.
- Fig. 7.30. Simulated supply side power quality performance of ASISEPIC Converter based Bidirectional LEV charger during G2V Mode and  $v_s$  of (a) 220 V, (b) 160 V, and (c) 265 V.
- Fig. 7.31. Experimental validation of supply side power quality performance of ASISEPIC Converter-based LEV charger during G2V and  $v_s$  of (a)-(c) 220 V (d)-(f) 165 V, and (g)-(i) 250 V.
- Fig. 7.32. Simulated Steady State Performance of ASISEPIC Converter-based Bidirectional LEV Charger during V2G Mode (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $i_{Li}$ ,  $v_{C1}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{Ss1}$ ,  $v_{Ss2}$ ,  $i_{Ss1}$ ,  $v_{Sa1}$ ,  $i_{Sa1}$ ,  $v_{Sa2}$ ,  $i_{Sa2}$ ,  $v_{Sa3}$ , and  $v_{Sa4}$ .

- Fig. 7.33. Experimental Steady State performance of ASISEPIC Converter based Bidirectional LEV charger during V2G Mode Operation (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ , and  $i_{bat}$  (b)  $v_s$ ,  $i_s$ ,  $i_{Li}$ , and  $v_{C1}$  (c)  $v_{Ss1}$ ,  $v_{Ss2}$ ,  $i_{Ls1}$ , and  $i_{Ls2}$  (d)  $v_s$ ,  $v_{S1}$ ,  $v_{Ss1}$ , and  $v_{Ss2}$  (e)  $v_{Sa1}$ ,  $v_{Sa2}$ ,  $v_{Sa3}$ , and  $v_{Sa4}$ .
- Fig. 7.34. Simulated performance of ASISEPIC Converter-based Bidirectional LEV charger during V2G Mode Operation under (a)-(b)  $v_s$  dynamics from (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub> and (c)-(d)  $i_{bat}$  dynamics from (c) 100% to 50%, and (d) 50% to 100% Conditions.
- Fig. 7.35. Experimental performance of ASISEPIC Converter-based Bidirectional LEV charger during V2G Mode Operation under (a)-(b)  $v_s$  dynamics from (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub> and (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub> and (c)-(d)  $i_{bat}$  dynamics from (c) 100% to 50%, and (d) 50% to 100% Conditions.
- Fig. 7.36. Simulated supply side power quality performance of ASISEPIC Converter-based Bidirectional LEV charger during V2G Mode and  $v_s$  of (a) 220 V, (b) 160 V, and (c) 265 V.
- Fig. 7.37. Experimental validation of supply side power quality performance of ASISEPIC Converter-based LEV charger during V2G and  $v_s$  of (a)-(c) 220 V (d)-(f) 165 V, and (g)-(i) 255 V.
- Fig. 8.1. FBLBSEPIC Converter based Bidirectional Single Stage Isolated LEV Charger.
- Fig. 8.2. FBLBL Converter based Bidirectional Single Stage Isolated LEV charger.
- Fig. 8.3. Equivalent Circuit of FBLBSEPIC Converter based Bidirectional LEV Charger during (a) Grid Connected Mode (G2V/V2G) and (b) Grid Disconnected Mode (V2H).
- Fig. 8.4. Line Cycle Operation of FBLBSEPIC Converter Based Bidirectional LEV Charger during G2V Operations (a) Positive, and (b) Negative Half Cycle of  $v_s$ .
- Fig. 8.5. Switching Cycle Operation of FBLBSEPIC Converter Based Bidirectional LEV Charger during G2V Operation (a) Mode – G2V(P<sub>1</sub>) (b) Mode – G2V(P<sub>2</sub>) and (c) Mode – G2V(P<sub>3</sub>)
- Fig. 8.6. Line Cycle Operation of FBLBSEPIC Converter Based Bidirectional LEV Charger during V2G Operation (a) Positive, and (b) Negative Half Cycle of  $v_s$ .
- Fig. 8.7. Switching Cycle Operation of FBLBSEPIC Converter Based Bidirectional LEV Charger during V2G Operation (a) Mode – V2G(P<sub>1</sub>) (b) Mode – V2G(P<sub>2</sub>) and (c) Mode – V2G(P<sub>3</sub>).
- Fig. 8.8. Switching Cycle Voltage/Current Waveforms of FBLBSEPIC Converter Based LEV Charger during (a) G2V and (b) V2G Mode Operation.
- Fig. 8.9. Equivalent Circuit of FBLBL Converter based Bidirectional LEV Charger during (a) Grid Connected Mode (G2V/V2G) and (b) Grid Disconnected Mode (V2H).
- Fig. 8.10. Line Cycle Operation of FBLBL Converter Based Bidirectional LEV Charger during G2V Operation (a) Positive (b) Negative Half Cycle of  $v_s$ .

- Fig. 8.11. Switching Cycle Operation of FBLBL Converter Based Bidirectional LEV Charger during G2V Operation (a) Mode – G2V(P<sub>1</sub>) (b) Mode – G2V(P<sub>2</sub>) and (c) Mode – G2V(P<sub>3</sub>)
- Fig. 8.12. Line Cycle Operation of FBLBL Converter Based Bidirectional LEV Charger during V2G Operation (a) Positive and (b) Negative Half Cycle of  $v_s$ .
- Fig. 8.13. Switching Cycle Operation of FBLBL Converter Based Bidirectional LEV Charger during V2G Operation (a) Mode – V2G(P<sub>1</sub>) (b) Mode – V2G(P<sub>2</sub>) and (c) Mode – V2G(P<sub>3</sub>).
- Fig. 8.14. Switching Cycle Voltage/Current Waveforms of FBLBL Converter Based LEV Charger during (a) G2V and (b) V2G Mode Operation.
- Fig. 8.15. Control Block Diagram for Bidirectional Single Stage Isolated LEV Chargers during (a) G2V/V2G and (b) V2H Mode Operation.
- Fig. 8.16. General Block Diagram for Software Modelling and MATLAB Simulation of Bidirectional Single Stage Isolated LEV Chargers.
- Fig. 8.17. Simulated Performance of FBLBSEPIC Converter-based Bidirectional LEV Charger Under Steady State G2V Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{C1}$ ,  $v_{C2}$ ,  $i_{pri1}$ ,  $i_{pri2}$ ,  $i_{sec1}$ , and  $i_{sec2}$  (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{S2}$ ,  $i_{S2}$ ,  $v_{So1}$ ,  $i_{So1}$ ,  $v_{So2}$ , and  $i_{So2}$ .
- Fig. 8.18. Experimental Performance of FBLBSEPIC Converter-based Bidirectional LEV Charger Under Steady State G2V Operating Conditions (a)  $v_s$ ,  $i_s$ ,  $i_{bat}$ , and  $v_{bat}$  (b)  $v_s$ ,  $v_{C2}$ ,  $v_{C1}$ , and  $v_{bat}$  (c)  $v_{S1}$ ,  $v_{S2}$ ,  $i_{pri1}$ , and  $i_{pri2}$  (d)  $v_{So1}$ ,  $v_{So2}$ ,  $i_{sec1}$ , and  $i_{sec2}$  (e)  $v_{S1}$ ,  $v_{S2}$ ,  $v_{So1}$ , and  $v_{So2}$ .
- Fig. 8.19. Simulated performance of FBLBSEPIC Converter-based Bidirectional LEV charger during G2V Mode and under (a)-(b)  $v_s$  dynamics (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub>, (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>, (c)-(d)  $i_{bat}$  dynamics (c) 100% to 50% and (d) 50% to 100%.
- Fig. 8.20. Experimental performance of FBLBSEPIC Converter based Bidirectional LEV charger during G2V Mode and under (a)-(b)  $v_s$  dynamics (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub>, (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>, (c)-(d)  $i_{bat}$  dynamics (c) 100% to 50% and (d) 50% to 100%.
- Fig.8.21. Simulated supply side power quality performance of FBLBSEPIC Converter based Bidirectional LEV charger during G2V Mode at  $P_{rated}$  and  $v_s$  of (a) 220 V, (b) 265 V, and (c) 160 V.
- Fig.8.22. Experimental supply side power quality performance of FBLBSEPIC Converter based Bidirectional LEV charger during G2V Mode at  $P_{rated}$  and  $v_s$  of (a) 220 V, (b) 265 V, and (c) 160 V.
- Fig. 8.23. Simulated Performance of FBLBSEPIC Converter-based Bidirectional LEV Charger Under Steady State V2G/V2H Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{C1}$ ,  $v_{C2}$ ,  $i_{pri1}$ ,  $i_{pri2}$ ,  $i_{sec1}$ , and  $i_{sec2}$  (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{S2}$ ,  $i_{S2}$ ,  $v_{So1}$ ,  $i_{So1}$ ,  $v_{So2}$ , and  $i_{So2}$ .
- Fig. 8.24. Experimental Performance of FBLBSEPIC Converter-based Bidirectional LEV Charger Under Steady State V2G Operating Conditions (a)  $v_s$ ,  $i_s$ ,  $i_{bat}$ , and  $v_{bat}$  (b)

$v_s$ ,  $v_{C2}$ ,  $v_{C1}$ , and  $v_{bat}$  (c)  $v_{S1}$ ,  $v_{S2}$ ,  $i_{pri1}$ , and  $i_{pri2}$  (d)  $v_{So1}$ ,  $v_{So2}$ ,  $i_{sec1}$ , and  $i_{sec2}$  (e)  $v_{S1}$ ,  $v_{S2}$ ,  $v_{So1}$ , and  $v_{So2}$ .

- Fig. 8.25. Performance of FBLBSEPIC Converter-based Bidirectional LEV Charger Under Steady State V2H Operating Conditions (a) Simulation ( $v_s$ ,  $i_s$ ,  $i_{bat}$ , and  $v_{bat}$ ) and (b) Experimental ( $v_s$ ,  $i_s$ ,  $i_{bat}$ , and  $v_{bat}$ ) Validation.
- Fig. 8.26. Simulated performance of FBLBSEPIC Converter-based Bidirectional LEV charger during V2G Mode and under (a)-(b)  $v_s$  dynamics (a) 220 V to 160 V, (b) 220 V to 265 V, (c)-(d)  $i_{bat}$  dynamics (c) 100% to 50% and (d) 50% to 100%.
- Fig. 8.27. Experimental performance of FBLBSEPIC Converter-based Bidirectional LEV charger during V2G Mode and under (a)-(b)  $v_s$  dynamics (a) 220 V to 160 V, (b) 220 V to 265 V, (c)-(d)  $i_{bat}$  dynamics (c) 100% to 50% and (d) 50% to 100%.
- Fig.8.28. Simulated supply side power quality performance of FBLBSEPIC Converter based Bidirectional LEV charger during (a)-(c) V2G Mode at  $P_{rated}$  and  $v_s$  of (a) 220 V, (b) 265 V, and (c) 160 V, and during (d) V2H Mode at  $v_s$  of 220 V.
- Fig.8.29. Experimental supply side power quality performance of FBLBSEPIC Converter based Bidirectional LEV charger during (a)-(i) V2G Mode at  $P_{rated}$  and  $v_s$  of (a)-(c) 220 V, (d)-(f) 265 V, and (g)-(i) 160 V.
- Fig. 8.30. Simulated Performance of FBLBL Converter based Bidirectional LEV Charger Under Steady State G2V Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{Cf1}$ ,  $v_{Cf2}$ ,  $i_{pri1}$ ,  $i_{pri2}$ ,  $i_{sec1}$ ,  $i_{sec2}$ ,  $v_{C1}$ , and  $i_{Lo}$  (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{S2}$ ,  $i_{S2}$ ,  $v_{So1}$ ,  $i_{So1}$ ,  $v_{So2}$ , and  $i_{So2}$ .
- Fig. 8.31. Experimental Performance of FBLBL Converter-based Bidirectional LEV Charger Under Steady State G2V Operating Conditions (a)  $v_s$ ,  $i_s$ ,  $i_{bat}$ , and  $v_{bat}$  (b)  $v_s$ ,  $v_{Cf1}$ ,  $v_{C1}$ , and  $i_{Lo}$  (c)  $v_{S1}$ ,  $v_{S2}$ ,  $i_{pri1}$ , and  $i_{pri2}$  (d)  $v_{So1}$ ,  $v_{So2}$ ,  $i_{sec1}$ , and  $i_{sec2}$  (e)  $v_{S1}$ ,  $v_{S2}$ ,  $v_{So1}$ , and  $v_{So2}$ .
- Fig. 8.32. Simulated performance of FBLBL-based LEV charger during G2V Mode (a)-(b)  $v_s$  dynamics (a) 220 V -160 V, (b) 220 V-265 V, (c)-(d)  $i_{bat}$  dynamics (c) 100% - 50% and (d) 50%-100%.
- Fig. 8.33. Experimental performance of FBLBL Converter based Bidirectional LEV charger during G2V Mode and under (a)-(b)  $v_s$  dynamics (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub>, (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>, (c)-(d)  $i_{bat}$  dynamics (c) 100% to 50% and (d) 50% to 100%.
- Fig.8.34. Simulated supply side power quality performance of FBLBL Converter based Bidirectional LEV charger during G2V Mode at  $P_{rated}$  and  $v_s$  of (a) 220 V, (b) 265 V, and (c) 160 V.
- Fig.8.35. Experimental supply side power quality performance of FBLBL Converter based Bidirectional LEV charger during G2V Mode at  $P_{rated}$  and  $v_s$  of (a) 220 V, (b) 265 V, and (c) 160 V.
- Fig. 8.36. Simulated Performance of FBLBL Converter-based Bidirectional LEV Charger Under Steady State V2G/V2H Operating Condition (a)  $v_s$ ,  $i_s$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $v_{Cf1}$ ,  $v_{Cf2}$ ,  $i_{pri1}$ ,  $i_{pri2}$ ,  $i_{sec1}$ ,  $i_{sec2}$ ,  $v_{C1}$ , and  $i_{Lo}$ , (b)  $v_s$ ,  $v_{S1}$ ,  $i_{S1}$ ,  $v_{S2}$ ,  $i_{S2}$ ,  $v_{So1}$ ,  $i_{So1}$ ,  $v_{So2}$ , and  $i_{So2}$ .

- Fig. 8.37. Experimental Performance of FBLBL Converter-based Bidirectional LEV Charger Under Steady State V2G Operating Conditions (a)  $v_s$ ,  $i_s$ ,  $i_{bat}$ , and  $v_{bat}$  (b)  $v_s$ ,  $v_{Cf1}$ ,  $v_{C1}$ , and  $i_{Lo}$  (c)  $v_{S1}$ ,  $v_{S2}$ ,  $i_{pri1}$ , and  $i_{pri2}$  (d)  $v_{So1}$ ,  $v_{So2}$ ,  $i_{sec1}$ , and  $i_{sec2}$  (e)  $v_{S1}$ ,  $v_{S2}$ ,  $v_{So1}$ , and  $v_{So2}$ .
- Fig. 8.38. Performance of FBLBL Converter-based LEV Charger Under Steady State V2H Operating Conditions (a) Simulation ( $v_s$ ,  $i_s$ ,  $i_{bat}$ , and  $v_{bat}$ ) and (b) Experimental ( $v_s$ ,  $i_s$ ,  $i_{bat}$ , and  $v_{bat}$ ) Validation.
- Fig. 8.39. Simulated performance of FBLBL-based LEV charger during V2G Mode under (a)-(b)  $v_s$  dynamics (a) 220 V–160 V, (b) 220 V–265 V, (c)-(d)  $i_{bat}$  dynamics (c) 100%-50% and (d) 50%-100%.
- Fig. 8.40. Experimental performance of FBLBL-based Bidirectional LEV charger during V2G Mode and under (a)-(b)  $v_s$  dynamics (a) 220 V<sub>RMS</sub> to 160 V<sub>RMS</sub>, (b) 220 V<sub>RMS</sub> to 265 V<sub>RMS</sub>, (c)-(d)  $i_{bat}$  dynamics (c) 100% to 50% and (d) 50% to 100%.
- Fig.8.41. Simulated supply side power quality performance of FBLBL Converter based Bidirectional LEV charger during (a)-(c) V2G Mode at  $P_{rated}$  and  $v_s$  of (a) 220 V, (b) 265 V, and (c) 160 V, and during (d) V2H Mode at  $v_s$  of 220 V.
- Fig.8.42. Experimental supply side power quality performance of FBLBL Converter based Bidirectional LEV charger during (a)-(i) V2G Mode at  $P_{rated}$  and  $v_s$  of (a)-(c) 220 V, (d)-(f) 265 V, and (g)-(i) 160 V.
- Fig. 9.1. ASIBB BDC-based Bidirectional Double Stage Non-isolated LEV Charger.
- Fig. 9.2. Equivalent Circuits of ASIBB BDC-based Bidirectional LEV Charger during (a) Grid to Vehicle (G2V), (b) Vehicle to Grid (V2G) and (c) Vehicle to Home (V2H) Mode Operation
- Fig. 9.3. Switching Cycle Operating Modes of ASIBB BDC Under (a)-(b) G2V Mode (a) *Mode–G2V(I)* ( $t_0 < t \leq t_1$ ) and (b) *Mode–G2V(II)* ( $t_1 < t \leq t_2$ ) and (c)-(d) V2G/V2H Mode (c) *Mode–V2G(I)* ( $t_0 < t \leq t_1$ ) and (d) *Mode–V2G(II)* ( $t_1 < t \leq t_2$ ).
- Fig. 9.4. Switching Cycle Voltage/Current Waveforms of ASIBB BDC Under (a) G2V and (b) V2G Mode Operations.
- Fig. 9.5. Control Architecture of Front-End AC-DC Stage of Bidirectional Double Stage Non-isolated LEV Charger (a) Generation of Reference Grid Current ( $i_g^*$ ) during G2V/V2G Modes, (b) Switching Logic during Mode Transition from G2V/V2G to V2H Mode, and during Grid Synchronization (c) Structure of SOSOGI QSG based FLL System.
- Fig. 9.6. Bode plots for (a) Inphase ( $v_{gp}$ ) to grid voltage ( $v_g$ ) and (b) Quadrature phase ( $v_{gq}$ ) to  $v_g$  Transfer functions of Presented Second Order SOGI OSG at  $k_1 = 1.56$ ,  $k_2 = 3.11$ , and  $w_g = 314.17$ .
- Fig. 9.7. Estimated Amplitude of  $v_g$  under (a) Distorted Grid Condition (10% 3rd Harmonic Content in  $v_g$ ) (b) DC offset Conditions (+15 V DC offset in  $v_g$ ), and (c)  $v_g$  Frequency Shift from 50 Hz to 47 Hz.

- Fig. 9.8. Estimated Frequency ( $\omega_g$ ) of  $v_g$  under (a) Distorted Grid Condition (10% 3<sup>rd</sup> Harmonics in  $v_g$ ) (b) DC offset Conditions (+15 V DC offset in  $v_g$ ), and (c)  $v_g$  Frequency Shift from 50 Hz to 47 Hz.
- Fig. 9.9. Control Block Diagram for Back End DC-DC Stage of Bidirectional Double Stage Non-isolated LEV Charger during (a) G2V/V2G and (b) V2H Mode Operation.
- Fig. 9.10. General Block Diagram for MATLAB Simulation and Performance Validation of Bidirectional Double Stage Non-isolated LEV Chargers.
- Fig. 9.11. Simulated Performance of ASIBB BDC based Bidirectional LEV Charger during Steady State G2V Mode Operation at (a)-(b) unity PF ( $Q_g^* = 0$  kVar), (a)  $v_g, i_g, v_{DC}, v_{bat}, i_{bat}, i_L, P_g, Q_g, P_L$  (b)  $v_{DC}, v_{bat}, i_{bat}, i_{Ls1}, i_{Ls2}, v_{S1}, i_{S1}, v_{Ss1}, i_{Ss1}, v_{Ss2}, i_{Ss2}$ .
- Fig. 9.12. Simulated Performance of ASIBB BDC based Bidirectional LEV Charger during Steady State V2G Mode Operation at unity PF ( $Q_g^* = 0$  kVar) Conditions (a)  $v_g, i_g, v_{DC}, v_{bat}, i_{bat}, i_L, P_g, Q_g, P_L, P_{bat}$  (b)  $v_{DC}, v_{bat}, i_{bat}, i_{Ls1}, i_{Ls2}, v_{S1}, i_{S1}, v_{Ss1}, i_{Ss1}, v_{Ss2}, i_{Ss2}$ .
- Fig. 9.13. Performance Validation of ASIBB BDC based Bidirectional LEV Charger during Steady State G2V Mode Operation at (a)-(e) unity PF ( $Q_g^* = 0$  kVar), (a)  $v_g, i_g, v_{DC}$  and  $i_{bat}$ , (b)  $v_g, i_g, v_{DC}, i_L$ , (c)  $P_g, Q_g, P_L, P_{bat}$  (d)  $v_{S1}, i_{Ls1}, i_{Ls2}, v_{Ss1}$  (e)  $v_{DC}, v_{S1}, v_{Ss1}, v_{Ss2}$ , and (f) Lagging PF ( $Q_g^* = +4$  kVar), and (g) Leading PF ( $Q_g^* = -4$  kVar) Conditions.
- Fig. 9.14. Performance Validation of ASIBB BDC based Bidirectional LEV Charger during Steady State V2G Mode Operation at (a)-(d) unity PF ( $Q_g^* = 0$  Var), (a)  $v_g, i_g, v_{DC}$  and  $i_{bat}$ , and (b)  $v_g, i_g, v_{DC}, i_L$ , (c)  $P_g, Q_g, P_L, P_{bat}$  (d)  $v_{S1}, i_{Ls1}, i_{Ls2}, v_{Ss1}$ , (e)  $v_{DC}, v_{S1}, v_{Ss1}, v_{Ss2}$ , and (f) Lagging PF ( $Q_g^* = +4$  kVar), and (g) Leading PF ( $Q_g^* = -4$  kVar) Conditions.
- Fig. 9.15. Performance Validation of ASIBB BDC-based Bidirectional LEV Charger during Steady State G2V Mode Operation at (a)  $V_{bat} = 36$  V and (b)  $V_{bat} = 240$  V.
- Fig. 9.16. Performance Validation of ASIBB BDC-based Bidirectional LEV charger under  $v_s$  dynamics (a)-(b) during G2V Mode Operation (a) from 240 V to 220 V, and (b) from 240 V to 265 V, and (c)-(d) during V2G Mode Operation (c) 240 V to 220 V, and (d) 240 V to 265 V.
- Fig. 9.17. Performance Validation of ASIBB BDC-based Bidirectional LEV charger under Change in  $i_{bat}$  from (a) Rated to 50% of Rated and (b) 50% of Rated to Rated Conditions during G2V, and from (c) Rated to 50% of Rated and (d) 50% of Rated to Rated Conditions during V2G Mode.
- Fig. 9.18. Performance Validation of ASIBB BDC-based Bidirectional LEV charger under Distorted Grid Conditions during (a) G2V and (b) V2G Mode Operation
- Fig. 9.19. Performance Validation of ASIBB BDC-based Bidirectional LEV charger during Change in Grid Frequency (a)-(b) under G2V Mode from (a) 50 Hz to 47 Hz (b) 50 Hz to 53 Hz, and (c)-(d) under V2G Mode from (c) 50 Hz to 47 Hz (d) 50Hz to 53 Hz.

- Fig. 9.20 Performance Validation of ASIBB BDC-based Bidirectional LEV charger under G2V-V2G and V2G-G2V Mode Transition
- Fig. 9.21 Performance of ASIBB BDC-based Bidirectional LEV Charger Under V2H Operating Conditions.
- Fig. 9.22 Experimental Performance of ASIBB BDC-based Bidirectional LEV Charger during Grid Disconnection and Reconnection Condition.
- Fig. 10.1 MSEPIC BDC based Bidirectional Double Stage Isolated LEV Charger.
- Fig. 10.2 Equivalent Circuits of MSEPIC Converter based Bidirectional LEV Charger under (a) Grid to Vehicle, (b) Vehicle to Grid, and (c) Vehicle to Home Mode Operation.
- Fig. 10.3 Switching Cycle Operating Modes of MSEPIC BDC during (a)-(b) G2V Mode Operation (a) Mode-G2V(I) ( $t_0 < t \leq t_1$ ) and (b) Mode-G2V(II) ( $t_1 < t \leq t_2$ ), and (c)-(d) during V2G/V2H Mode Operation (a) Mode-V2G(I) ( $t_0 < t \leq t_1$ ) and (b) Mode-V2G(II) ( $t_1 < t \leq t_2$ ).
- Fig. 10.4 Switching Cycle Voltage/Current Waveforms of MSEPIC BDC during (a) G2V and (b) V2G/V2H Mode Operations.
- Fig. 10.5 Control Architecture of Front-End AC-DC Stage of Bidirectional Double Stage Isolated LEV Charger (a) Generation of Reference Grid Current ( $i_g^*$ ) during G2V/V2G Modes, (b) Switching Logic during Mode Transition from G2V/V2G to V2H Mode, and during Grid Synchronization (c) Structure of IMSTOGI QSG based PLL System.
- Fig. 10.6 Control Architecture of Back End DC-DC Stage of Bidirectional Double Stage Isolated LEV Charger.
- Fig. 10.7 General Block Diagram for Software Modelling and MATLAB Simulation of Bidirectional Double Stage Isolated LEV Chargers.
- Fig. 10.8 Simulated Performance of MSEPIC BDC based Bidirectional LEV Charger during Steady State G2V Mode Operation (at  $P_g^* = +7.2$  kW and  $Q_g^* = 0$  kVar) (a)  $v_g$ ,  $i_g$ ,  $v_{DC}$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $i_L$ ,  $P_g$ ,  $Q_g$ ,  $P_L$ , and  $P_{bat}$  (b)  $v_{DC}$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $i_{Li}$ ,  $i_{Lo}$ ,  $v_{CI}$ ,  $v_{Cs1}$ ,  $v_{Cs2}$ ,  $v_{S1}$ ,  $v_{Ss1}$ , and  $v_{Ss2}$ .
- Fig. 10.9 Performance Validation of MSEPIC BDC based Bidirectional LEV Charger during Steady State G2V Mode Operation (at  $P_g^* = +7.2$  kW and  $Q_g^* = 0$  kVar) (a)  $v_g$ ,  $i_g$ ,  $v_{DC}$ , and  $i_{bat}$ , and (b)  $v_g$ ,  $i_g$ ,  $v_{DC}$  and  $i_L$ , (c)  $P_g$ ,  $Q_g$ ,  $P_L$ , and  $P_{bat}$  (d)  $v_{DC}$ ,  $v_{S1}$ ,  $v_{Ss1}$ , and  $v_{Ss2}$  (e)  $i_{Li}$ ,  $i_{Lo}$ ,  $v_{CI}$ , and  $v_{Cs1}$ .
- Fig. 10.10 Simulated Performance of MSEPIC BDC based Bidirectional LEV Charger during Steady State V2G Mode Operation (at  $P_g^* = -6$  kW and  $Q_g^* = 0$  kVar) (a)  $v_g$ ,  $i_g$ ,  $v_{DC}$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $i_L$ ,  $P_g$ ,  $Q_g$ ,  $P_L$ , and  $P_{bat}$  (b)  $v_{DC}$ ,  $v_{bat}$ ,  $i_{bat}$ ,  $i_{Li}$ ,  $i_{Lo}$ ,  $v_{CI}$ ,  $v_{Cs1}$ ,  $v_{Cs2}$ ,  $v_{S1}$ ,  $v_{Ss1}$ , and  $v_{Ss2}$ .
- Fig. 10.11 Performance Validation of MSEPIC BDC based Bidirectional LEV Charger during Steady State V2G Mode Operation (at  $P_g^* = -6$  kW and  $Q_g^* = 0$  kVar) (a)  $v_g$ ,  $i_g$ ,  $v_{DC}$  and  $i_{bat}$ , and (b)  $v_g$ ,  $i_g$ ,  $v_{DC}$  and  $i_L$ , (c)  $P_g$ ,  $Q_g$ ,  $P_L$ , and  $P_{bat}$  (d)  $v_{DC}$ ,  $v_{S1}$ ,  $v_{Ss1}$ , and  $v_{Ss2}$  (e)  $i_{Li}$ ,  $i_{Lo}$ ,  $v_{CI}$ , and  $v_{Cs1}$ .

- Fig. 10.12 Performance Validation of MSEPIC BDC based Bidirectional LEV charger under  $v_g$  dynamics during (a)-(b) G2V Mode Operation from (a) 240  $V_{RMS}$  to 220  $V_{RMS}$ , and (b) 240  $V_{RMS}$  to 265  $V_{RMS}$ , and (c)-(d) V2G Mode Operation (c) 240  $V_{RMS}$  to 220  $V_{RMS}$ , and (d) 240  $V_{RMS}$  to 265  $V_{RMS}$ .
- Fig. 10.13 Performance Validation of MSEPIC BDC based Bidirectional LEV charger during Change in  $P_g^*$  ( $Q_g^* = 0$  kVar) (a)-(b) during G2V Mode (a) from +7.2 kW to +3.6 kW (b) from +3.6 kW to +7.2 kW, and (c)-(d) during V2G Mode (c) from -6 kW to -3kW, and (d) from -3 kW to -6 kW.
- Fig. 10.14 Performance Validation of MSEPIC BDC based Bidirectional LEV charger under Change in  $Q_g^*$  (a)-(b) during G2V ( $P_g^* = +3.6$  kW) (a) from 0 kVar to +4 kVar and (b) from 0 kVar to -4 kVar and (c)-(d) during V2G ( $P_g^* = -3$  kW) (c) from 0 kVar to +2 kVar and (d) from 0 kVar to -2 kVar.
- Fig.10.15 Performance Validation of MSEPIC BDC based Bidirectional LEV charger under Distorted Grid Condition during (a) G2V and (b) V2G Mode Operation.
- Fig. 10.16 Performance Validation of MSEPIC BDC based Bidirectional LEV charger under (a) G2V to V2G and (b) V2G to G2V Mode Transition.
- Fig. 10.17 Performance Validation of MSEPIC BDC based Bidirectional LEV Charger Under V2H Operating Conditions.
- Fig. 10.18 Performance Validation of MSEPIC BDC based Bidirectional LEV Charger during (a) Grid Disconnection and (b)-(c) Grid Reconnection Conditions.

## LIST OF TABLES

Table 1.1	Charging Standards and Levels
Table 3.1	Switching Cycle Voltage/Current Expressions for BSIC PFC AC-DC Converter
Table 3.2	Switching Cycle Voltage/Current Expressions for BSISEPIC PFC AC-DC Converter
Table 3.3	Design Specifications for BSIC and BSISEPIC PFC AC-DC Converter Based Chargers
Table 3.4	Comparison Between BSIC and BSISEPIC PFC AC-DC Converter Based Unidirectional Single Stage Nonisolated LEV Chargers
Table 4.1	Switching Cycle Voltage/Current Expressions for FBLPOBB PFC AC-DC Converter
Table 4.2	Switching Cycle Voltage/Current Expressions for BLPOL PFC AC-DC Converter
Table 4.3	Switching Cycle Voltage/Current Expressions for FBLPOL PFC AC-DC Converter
Table 4.4	Switching Cycle Voltage/Current Expressions for BLSEPIC PFC AC-DC Converter
Table 4.5	Switching Cycle Voltage/Current Expressions for BLPOC PFC AC-DC Converter
Table 4.6	Switching Cycle Voltage/Current Expressions for BLMSEPIC PFC AC-DC Converter
Table 4.7	Design Specifications for FBLPOBB PFC AC-DC Converter based LEV Charger
Table 4.8	Design Specifications for BLPOL PFC AC-DC Converter based LEV Charger
Table 4.9	Design Specifications for FBLPOL PFC AC-DC Converter based LEV Charger
Table 4.10	Design Specifications for BLSEPIC PFC AC-DC Converter based LEV Charger
Table 4.11	Design Specifications for BLPOC PFC AC-DC Converter based LEV Charger
Table 4.12	Design Specifications for BLMSEPIC PFC AC-DC Converter based LEV Charger
Table 4.13	Comparison Between Unidirectional Single Stage Isolated LEV Chargers
Table 5.1	Switching Cycle Voltage/Current Expressions for PBLCSC PFC AC-DC Converter
Table 5.2	Switching Cycle Voltage/Current Expressions for HGB DC-DC Converter
Table 5.3	Steady State Expressions for HGB DC-DC Converter
Table 5.4	Switching Cycle Voltage/Current Expressions for FBLCSC PFC AC-DC Converter
Table 5.5	Design Specifications for PBLCSC and FBLCSC PFC-Based LEV Chargers
Table 5.6	Selection of Reference DC Link Voltage LEV
Table 5.7	Comparison Between PBLCSC and FBLCSC PFC AC-DC Converter Based Unidirectional Double Stage Nonisolated LEV Chargers
Table 6.1	Switching Cycle Voltage/Current Expressions for ILCSC PFC AC-DC Converter
Table 6.2	Switching Cycle Voltage/Current Expressions for IPOC DC-DC Converter

Table 6.3	Switching Cycle Voltage/Current Expressions for MSCCSC PFC AC-DC Converter
Table 6.4	Design Specifications for Double Stage Isolated Based LEV Charger
Table 6.5	Comparison Between ILCSC and MSCCSC PFC AC-DC Converter Based Unidirectional Double Stage Isolated LEV Chargers
Table 7.1	Switching Cycle Voltage/Current Expressions for ASIC Converter (During G2V Mode)
Table 7.2	Switching Cycle Voltage/Current Expressions for ASIC Converter (During V2G Mode)
Table 7.3	Switching Cycle Voltage/Current Expressions for SISEPIC Converter (G2V Mode)
Table 7.4	Switching Cycle Voltage/Current Expressions for SISEPIC Converter (V2G Mode)
Table 7.5	Design Specifications for ASIC and ASISEPIC Converter-based Bidirectional Chargers
Table 7.6	Design and Selection of ASIC and ASISEPIC Converter based Chargers' Component
Table 7.7	Comparison Between ASIC and ASISEPIC Converter Based Bidirectional Single Stage Nonisolated LEV Chargers
Table 8.1	Switching Cycle Voltage/Current Expressions for FBLBSEPIC Converter (G2V Mode)
Table 8.2	Switching Cycle Voltage/Current Expressions for FBLBSEPIC Converter (V2G Mode)
Table 8.3	Switching Cycle Voltage/Current Expressions for FBLBL Converter (G2V Mode)
Table 8.4	Switching Cycle Voltage/Current Expressions for FBLBL Converter (V2G Mode)
Table 8.5	Design Specifications for FBLBSEPIC and FBLBL-based Bidirectional Charger
Table 8.6	Design and Selection of FBLBSEPIC Converter-based Charger's Components
Table 8.7	Design and Selection of FBLBL Converter-based Charger's Components
Table 9.1	Switching Cycle Voltage/Current Expressions for ASIBB BDC (during G2V)
Table 9.2	Switching Cycle Voltage/Current Expressions for ASIBB BDC (during V2G)
Table 9.3	Design Specifications for ASIBB BDC-based Bidirectional LEV Charger
Table 10.1	Switching Cycle Electrical Expressions for MSEPIC BDC (during G2V)
Table 10.2	Switching Cycle Electrical Expressions for MSEPIC BDC (during V2G/V2H)
Table 10.3	Steady State Expressions for MSEPIC BDC
Table 10.4	Specifications for MSEPIC BDC based Bidirectional LEV Charger

## LIST OF ABBREVIATIONS

AC	Alternating Current
ADC	Analog to Digital Controller
ASIBB	Active Switched Inductor Buck-Boost
ASIC	Active Switched Inductor Cuk
ASISEPIC	Active Switched Inductor SEPIC
BDC	Bidirectional DC-DC Converter
BEV	Battery Electric Vehicle
BLPOC	Bridgeless Positive Output Cuk
BLPOL	Bridgeless Positive Output Luo
BSIC	Bridgeless Switched Inductor Cuk
BLSEPIC	Bridgeless SEPIC
BLMSEPIC	Bridgeless Modified SEPIC
BSISEPIC	Bridgeless Switched Inductor SEPIC
CC	Constant Current
CCM	Continuous Conduction Mode
CP	Constant Power
CrCM	Critical Conduction Mode
CSC	Canonical Switching Cell
CV	Constant Voltage
DAB	Dual Active Bridge
DBR	Diode Bridge Rectifier
DC	Direct Current
DCM	Discontinuous Conduction Mode
DF	Displacement Factor
DIS	Domestic Inverter System
DSO	Digital Signal Oscilloscope
E2W	Electric Two-Wheeler
E3W	Electric Three-Wheeler
E4W	Electric Four-Wheeler
EMC	Electromagnetic Compatibility
EMI	Electromagnetic Interference
EPWM	Enhanced Pulse Width Modulation
EV	Electric Vehicle
FBLBSEPIC	Fully Bridgeless Bidirectional SEPIC
FBLBL	Fully Bridgeless Bidirectional Luo
FBLCSC	Fully Bridgeless CSC
FBLPOBB	Fully Bridgeless Positive Output Buck-Boost
FBLPOL	Fully Bridgeless Positive Output Luo
FLL	Frequency Locked Loop
GaN	Gallium Nitride
GI	Generalized Integrator

G2V	Grid to Vehicle
HEV	Hybrid Electric Vehicle
HGB	High Gain Buck
HVBEV	High Voltage Battery Electric Vehicle
IC	Integrated Circuit
ICE	Internal Combustion Engine
IEC	International Electrotechnical Commission
IEEE	Institute of Electrical and Electronics Engineers
IGBT	Insulated Gate Bipolar Transistor
ILCSC	Interleaved CSC
IM	Inductor Motor
IMSTOGI	Improved Mixed Second and Third-Order Generalized Integrator
IPOC	Isolated Positive Output Cuk
kWh	Kilo-Watt-Hour
LEV	Light Electric Vehicle
LPF	Low Pass Filter
LVBEV	Low Voltage Battery Electric Vehicle
MSCCSC	Modified Switched Capacitor CSC
MSEPIC	Modified SEPIC
MTS	Mode Transfer Switch
OBC	On Board Charger
OSG	Orthogonal Signal Generator
PBLCSC	Partial Bridgeless CSC
PF	Power Factor
PFC	Power Factor Corrected
PHEV	Plugin Hybrid Electric Vehicle
PI	Proportional-Integral
PLL	Phased Locked Loop
PMBLDCM	Permanent Magnet Brushless DC Motor
PMSM	Permanent Magnet Synchronous Motor
PQ	Power Quality
PR	Proportional Resonant
QSG	Quadrature Signal Generator
RCD	Resistor Capacitor Diode
RMS	Root Mean Square
SAE	Society of Automotive Engineers
SEPIC	Single Ended Primary Inductor Converter
SIC	Silicon Carbide
SOC	State of Charge
SOGI	Second Order Generalized Integrator
SOH	State of Health
SOSOGI	Second Order SOGI
SRF	Synchronous Reference Frame

SRM	Switched Reluctance Motor
THD	Total Harmonics Distortions
TI	Texas Instrument
VRLA	Valve Regulated Lead Acid
VSI	Voltage Source Inverter
VTR	Voltage Transfer Ratio
V2G	Vehicle to Grid
V2H	Vehicle to Home
V2L	Vehicle to Load
V2V	Vehicle to Vehicle
V2X	Vehicle to Anything
1P1S	One Primary and One Secondary
1P2S	One Primary and Two Secondary
2P2S	Two Primary and Two Secondary
2P1S	Two Primary and One Secondary

## LIST OF SYMBOLS

$C_1, C_2, C_3$	Intermediate Energy Transfer Capacitors
$C_{1c}$	Primary Side Capacitor of Isolated Cuk Converter
$C_{2c}$	Secondary Side Capacitor of Isolated Cuk Converter
$C_{DC}$	DC Link Capacitor
$C_o$	Battery End Filter Capacitor
$C_f, C_{f1}, C_{f2}$	Supply Side Filter Capacitor
$C_{s1}, C_{s2}$	Capacitors of Switched Capacitor Cell
$D_1, D_2, D_3, D_4$	High frequency Diodes
$D_b$	Duty Ratio of back end DC-DC Converter switch
$D_c, D_{c1}, D_{c2}$	Diodes of Cuk Converter
$D_D$	Diode Duty Ratio
$D_{Dcr}$	Critical Value of Diode Duty Ratio
$D_{G2V}$	Duty Ratio of back end DC-DC Converter switch (G2V Mode)
$D_{s1}, D_{s2}$	Diodes of Switched Inductor/Capacitor Cell
$D_S$	Switch Duty Ratio
$D_{Smin}$	Minimum Value of $D_S$
$D_{Smax}$	Maximum Value of $D_S$
$D_{V2G}$	Duty Ratio of back end DC-DC Converter switch (V2G Mode)
$D_{b1}, D_{b2}, D_{b3}, D_{b4}$	Diodes of Diode Bridge Rectifier
$D_o, D_{o1}, D_{o2}$	Output Diodes at Secondary Side of Transformer
$f_L$	Line Frequency
$f_s$	Switching Frequency
$f_{sb}$	Switching frequency of Back end DC-DC converter
$G_C$	DC Gain of Isolated Cuk DC-DC Converter
$G_{HGB}$	DC Gain of High Gain Buck (HGB) DC-DC Converter
$i_{bat}$	Battery Current
$I_{bat}$	Average Value of $i_{bat}$
$I_{batmin}$	Minimum value of $I_{bat}$
$I_{batmax}$	Maximum value of $I_{bat}$
$I_{bat}^*$	Reference Battery Current
$i_{bate}$	Error between $i_{bat}$ and $I_{bat}^*$
$i_{Co}$	Current through $C_o$

$i_{DC}$	DC Link Current
$I_{in}$	Switching cycle average value of $i_s$
$i_{Ls1}, i_{Ls2}$	Current through $L_{s1}, L_{s2}$
$I_{Ls1RMS}, I_{Ls2RMS}$	RMS Current through $L_{s1}, L_{s2}$
$I_{Ls1}, I_{Ls2}$	Switching Cycle Average value of $i_{Ls1}, i_{Ls2}$
$i_s$	Instantaneous Supply Current
$I_s$	RMS Value of $i_s$
$I_{smin}$	Minimum value of $I_s$
$I_{smax}$	Maximum value of $I_s$
$i_{Cs1}, i_{Cs2}$	Current through $C_{s1}, C_{s2}$
$i_{Ds1}, i_{Ds2}$	Current through $D_{s1}, D_{s2}$
$i_{Ds1peak}, i_{Ds2peak}$	Peak Current through $D_{s1}, D_{s2}$
$I_{Ds1RMS}, I_{Ds2RMS}$	RMS Current through $D_{s1}, D_{s2}$
$I_{Ds1}, I_{Ds2}$	Switching Cycle Average value of $i_{Ds1}, i_{Ds2}$
$i_{Ss1}, i_{Ss2}$	Current through $S_{s1}, S_{s2}$
$i_{Sa1}, i_{Sa2}, i_{Sa3}, i_{Sa4}$	Current through $S_{a1} - S_{a4}$
$i_{Lm}, i_{Lm1}, i_{Lm2}$	Current through $L_m, L_{m1}, L_{m2}$
$i_{pri}, i_{pri1}, i_{pri2}$	Current through primary windings of $T_x, T_{x1}, T_{x2}$
$i_{sec}, i_{sec1}, i_{sec2}$	Current through secondary windings of $T_x, T_{x1}, T_{x2}$
$i_{Lic}$	Current through $L_{ic}$
$i_{Loc}$	Current through $L_{oc}$
$i_{C1c}$	Current through $C_{1c}$
$i_{C2c}$	Current through $C_{2c}$
$i_{Sc}, i_{Sc1}, i_{Sc2}$	Current through $S_c, S_{c1}, S_{c2}$
$i_{Dc}, i_{Dc1}, i_{Dc2}$	Current through $D_c, D_{c1}, D_{c2}$
$i_{Db1}, i_{Db2}, i_{Db3}, i_{Db4}$	Current through $D_{b1}, D_{b2}, D_{b3}, D_{b4}$
$i_{Db1/Db2/Db3/Db4peak}$	Peak Current through $D_{b1}, D_{b2}, D_{b3}, D_{b4}$
$I_{Db1/Db2/Db3/Db4RMS}$	RMS Current through $D_{b1}, D_{b2}, D_{b3}, D_{b4}$
$i_{C1}, i_{C2}, i_{C3}$	Current through $C_1, C_2, C_3$
$i_{Li}, i_{Li1}, i_{Li2}$	Current through $L_i, L_{i1}, L_{i2}$
$i_{Lo}$	Current through $L_o$
$i_{Do}, i_{Do1}, i_{Do2}$	Current through $D_o, D_{o1}, D_{o2}$
$i_{Do/Do1/Do2peak}$	Peak Current through $D_o, D_{o1}, D_{o2}$

$I_{D_o/D_{o1}/D_{o2}RMS}$	RMS Current through $D_o, D_{o1}, D_{o2}$
$i_{D1}, i_{D2}, i_{D3}, i_{D4}$	Current through $D_1, D_2, D_3, D_4$
$i_{D1/D2/D3/D4peak}$	Peak Current through $D_1, D_2, D_3, D_4$
$I_{D1/D2/D3/D4RMS}$	Peak Current through $D_1, D_2, D_3, D_4$
$i_{S1}, i_{S2}, i_{S3}, i_{S4}$	Current through $S_1, S_2, S_3, S_4$
$i_{S1/S2/S3/S4peak}$	Peak Current through $S_1, S_2, S_3, S_4$
$I_{S1/S2/S3/S4RMS}$	RMS Current through $S_1, S_2, S_3, S_4$
$I_{S1}, I_{S2}, I_{S3}, I_{S4}$	Average Current through $S_1, S_2, S_3, S_4$
$L_{eq}$	Equivalent Inductance of $L_i$ and $L_{s1}/L_{s2}$
$L_g$	Supply Impedance
$L_f, L_{f1}, L_{f2}$	Supply Side Filter Inductor
$L_{s1}, L_{s2}$	Inductors of Switched Inductor Cell
$L_s$	Switched Inductor Inductance Considering $L_{s1} = L_{s2}$
$L_{scr}$	Critical Value of $L_s$
$L_m, L_{m1}, L_{m2}$	Magnetizing Inductance of $T_x, T_{x1}, T_{x2}$
$L_{mcr}$	Critical Value of $L_m, L_{m1}, L_{m2}$
$L_{ic}$	Input Inductor of Isolated Cuk Converter
$L_i, L_{i1}, L_{i2}$	Input Inductors
$L_{icr}, L_{i1cr}, L_{i2cr}$	Critical values of $L_i, L_{i1}, L_{i2}$
$L_{oc}$	Output Inductor of Isolated Cuk Converter
$L_o$	Output Inductor
$L_{ocr}$	Critical Values of $L_o$
$M_{VDC}$	Switching Cycle DC Voltage Gain of Converters
$M_{IDC}$	Switching Cycle DC Current Gain of Converters
$M_{VDCmin}$	Minimum value of $M_{VDC}$
$M_{VDCmax}$	Maximum value of $M_{VDC}$
$N$	Primary to Secondary Turns Ratio of $T_x, T_{x1}, T_{x2}$
$N_{pri}, N_{pri1}, N_{pri2}$	Number of Primary turns of $T_x, T_{x1}, T_{x2}$
$N_{sec}, N_{sec1}, N_{sec2}$	Number of Secondary turns of $T_x, T_{x1}, T_{x2}$
$P_{rated}$	Rated power level of Charger
$R_f$	AC Side R-C Filter's Resistance
$R_L$	Fictitious Load Resistance
$R_{Lmin}$	Minimum value of $R_L$

$R_{Lmax}$	Maximum value of $R_L$
$R_{in}$	Fictitious Input Resistance
$S_1, S_2, S_3, S_4$	Switches
$S_{s1}, S_{s2}$	Switches of Active Switched Inductor/Capacitor Cell
$S_{a1}, S_{a2}, S_{a3}, S_{a4}$	Active Full Bridge AC-DC Converter Switches
$S_c, S_{c1}, S_{c2}$	Switches of Cuk Converter
$T_x, T_{x1}, T_{x2}$	High Frequency Transformers
$T_s$	Switching Time Period
$v_{bat}$	Battery Voltage
$V_{bat}$	Switching Cycle Average Value of $v_{bat}$
$V_{bat}^*$	Reference Battery Voltage
$v_{bate}$	Error between $v_{bat}$ and $V_{bat}^*$
$V_{batn}$	Nominal voltage of battery packs
$V_{batmin}$	Minimum Nominal voltage of battery packs
$V_{batmax}$	Maximum Nominal voltage of battery packs
$v_{Cf}, v_{Cf1}, v_{Cf2}$	Voltage across $C_f, C_{f1}, C_{f2}$
$v_{DC}$	DC Link Voltage
$V_{DC}^*$	Reference DC Link Voltage
$v_s$	Instantaneous Supply Voltage
$V_s$	RMS Value of $v_s$
$V_{smin}$	Minimum value of $V_s$
$V_{smax}$	Maximum value of $V_s$
$V_{in}$	Switching Cycle Average Value of $v_s$
$v_{Ls1}, v_{Ls2}$	Voltage across $L_{s1}, L_{s2}$
$v_{Cs1}, v_{Cs2}$	Voltage across $C_{s1}, C_{s2}$
$v_{Ds1}, v_{Ds2}$	Voltage across $D_{s1}, D_{s2}$
$v_{Ss1}, v_{Ss2}$	Voltage across $S_{s1}, S_{s2}$
$v_{Sa1}, v_{Sa2}, v_{Sa3}, v_{Sa4}$	Voltage Across $S_{a1} - S_{a4}$
$v_{pri}, v_{pri1}, v_{pri2}$	Voltage across primary windings of $T_x, T_{x1}, T_{x2}$
$v_{sec}, v_{sec1}, v_{sec2}$	Voltage across secondary windings of $T_x, T_{x1}, T_{x2}$
$v_{Lic}$	Voltage across $L_{ic}$
$v_{Loc}$	Voltage across $L_{oc}$
$v_{C1c}$	Voltage across $C_{1c}$

$v_{C2c}$	Voltage across $C_{2c}$
$v_{Sc}, v_{Sc1}, v_{Sc2}$	Voltage across $S_c, S_{c1}, S_{c2}$
$v_{Dc}, v_{Dc1}, v_{Dc2}$	Voltage across $D_c, D_{c1}, D_{c2}$
$v_{C1}, v_{C2}, v_{C3}$	Voltage across $C_1, C_2, C_3$
$V_{C1}, V_{C2}, V_{C3}$	Switching Cycle Average Voltage across $C_1, C_2, C_3$
$v_{Li}, v_{Li1}, v_{Li2}$	Voltage across $L_i, L_{i1}, L_{i2}$
$v_{Lo}$	Voltage across $L_o$
$v_{Db1/Db2/Db3/Db4}$	Voltage across $D_{b1}, D_{b2}, D_{b3}, D_{b4}$
$v_{S1}, v_{S2}, v_{S3}, v_{S4}$	Voltage across $S_1, S_2, S_3, S_4$
$v_{S1/S2/S3/S4peak}$	Peak Voltage stress across $S_1, S_2, S_3, S_4$
$v_{D1}, v_{D2}, v_{D3}, v_{D4}$	Voltage across $D_1, D_2, D_3, D_4$
$v_{Do}, v_{Do1}, v_{Do2}$	Voltage across $D_o, D_{o1}, D_{o2}$
$\gamma_{Li}$	Percentage Ripple in $L_i$ Current
$\gamma_{Ls}$	Percentage Ripple in $L_{s1}$ and $L_{s2}$ Currents
$\gamma_{Lic}$	Percentage Ripple in $L_{ic}$ Current
$\gamma_{Li1}$	Percentage Ripple in $L_{i1}$ Current
$\gamma_{Li2}$	Percentage Ripple in $L_{i2}$ Current
$\alpha_{C1c}$	Percentage Ripple in $C_{1c}$ Voltage
$\alpha_{C2c}$	Percentage Ripple in $C_{2c}$ Voltage
$\xi$	Percentage Ripple in Cuk Converter Transformer $i_{Lm}$
$\beta$	Percentage Ripple in $v_{C2}$
$\delta$	Percentage Ripples in $v_{DC}$
$\chi$	Percentage Ripple in $v_{C1}$
$\varphi$	Output Inductor Current Ripples $i_{Lo}$
$\kappa$	Percentage Ripples in $v_{Cs}$
$\lambda$	Percentage Ripples in $v_{Co}$
$\omega_{res}, \omega_{res1}, \omega_{res2}$	Resonance Frequency
$\Psi$	Percentage of Source Impedance
$f_c$	Cutoff frequency of filter