

**ELECTRICAL BEHAVIOR OF PARTIALLY SATURATED
CEMENT PASTE, MORTAR AND CONCRETE SUBJECTED TO
RADIO FREQUENCY EXCITATION**

GOPINANDAN DEY



**DEPARTMENT OF CIVIL ENGINEERING
INDIAN INSTITUTE OF TECHNOLOGY DELHI
SEPTEMBER 2019**

© Indian Institute of Technology Delhi (IITD), New Delhi, 2019

**ELECTRICAL BEHAVIOR OF PARTIALLY SATURATED
CEMENT PASTE, MORTAR AND CONCRETE SUBJECTED
TO RADIO FREQUENCY EXCITATION**

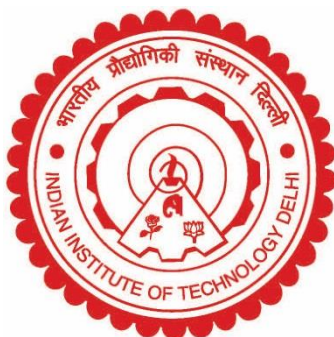
GOPINANDAN DEY

DEPARTMENT OF CIVIL ENGINEERING

Submitted

in fulfilment of the requirements of the degree of Doctor of Philosophy

to the



INDIAN INSTITUTE OF TECHNOLOGY DELHI

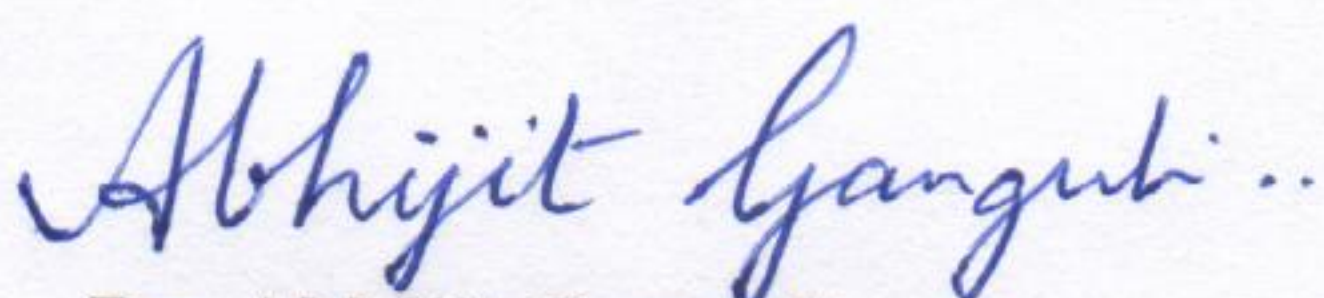
SEPTEMBER 2019

THE THESIS HAS BEEN DEDICATED TO MY FAMILY

CERTIFICATE

This is to certify that the thesis entitled “**Electrical Behavior of Partially Saturated Cement Paste, Mortar and Concrete Subjected to Radio Frequency Excitation**” being submitted by **Mr. Gopinandan Dey** to the Indian Institute of Technology Delhi is a record of bonafide research work carried out by him under our supervision and guidance. The thesis work, in our opinion, has reached the standard, fulfilling the requirements for the award of **Doctor of Philosophy** degree.

The research report and results presented in this thesis have not been submitted, in part or full, to any University or Institute for the award of any degree or diploma.



Dr. Abhijit Ganguli
Associate Professor
Department of Civil Engineering
Indian Institute of Technology Tirupati
Andhra Pradesh

Prof. Bishwajit Bhattacharjee
Professor
Department of Civil Engineering
Indian Institute of Technology Delhi
New Delhi

Dr. Tapan Kumar Gandhi
Assistant Professor
Department of Electrical Engineering
Indian Institute of Technology Delhi
New Delhi

Acknowledgements

I owe my deepest gratitude to my thesis supervisor, Dr. Abhijit Ganguli, who exemplifies the virtues of hard work and dedication, whose energy and empathy are limitless, and whose patience in meticulously proofreading the numerous revisions of my papers continues to amaze me. His wisdom, insight, and comprehensive approach to the problem have contributed greatly to this thesis and to my intellectual development. I also owe my thankfulness to my other supervisors Professor Bishwajit Bhattacharjee and Dr. Tapan Kumar Gandhi for their immense guidance throughout the period of this work. I hope this work is only the prelude to an enduring friendship and future research collaboration.

I am grateful to my Student Research Committee (SRC) members, Professors J. T. Sahoo, Dr. A. K. Swamy and Dr. K. Khare for their time, comments, and suggestions. I also thank help and instructive discussions with Late Goutam Barai Technical Superintendent of Materials Research laboratory of Indian Institute of Technology Delhi. I would like to express my gratitude to Mr Lal Singh and Mr Biri Singh for extending their helping hand to access their laboratories for sample preparation for this work.

I would also like to thank my colleagues Surendra, Debdutta, Gautham, Gopala, Vineet, Sreejith, Arun and Nabeel who have helped me, whenever I required, with dedication during the experiments at various stages. The liberty of managing the lab hours was made possible with due help from Nitin Chourasia, thanks to him. My sincere thanks to the people in the laboratory, specially Ganesh, Vinesh and Rajender, Ramesh, Sanjay and Sanjay and others who helped with dedication for preparing my experimental samples.

I am indebted to my parents-in law for their everlasting support. Their emotional support to me and my family during this entire period of PhD studies made this work possible. I am ever indebted to my wife Parbati for her constant support and inspiration, without which my dream would have remained unfulfilled. I am also thankful to my sons, Abhranil and Abhiroop for their unspeakable sufferings during our stay in Delhi. There are not enough words with which I can

thank my domestic helper Saraswati for her support throughout all these years. I am also grateful to my parents who had lost my companion for a long period during my PhD study. I would also like to thank my colleagues in NIT Agartala Rajib, Sima, Joyanta, Dipankar, Partha, Lipika, Rama, Ratul da and Abaniswar and others who were always my source of inspiration. Special thanks to Manish da who has always been my motivator in life with his valuable advice.

At the end I would like to give a very special thanks to NIT Agartala authority, Civil Engineering Department and QIP center of IIT Delhi for extending me the facility to pursue PhD in such a great institution.

Abstract

Cement based materials (CBMs) are porous and constitute a significant portion of materials used in construction in the form of cement concrete, cement mortar or cement paste. The porous nature of CBMs facilitate moisture movement through the pores which also act as a conduit for aggressive chemicals. All degrading chemical reactions occur in the presence of moisture that may originate from a variety of sources such as rainwater, surface water or ground water. The transport property of the material and the susceptibility to the diffusion of aggressive chemicals are dependent on the degree of saturation (DoS) and for assessments of not only the gross DoS but information of its temporal variation and spatial distribution in the material are essential. This enables identification of the level of vulnerability of the material to a probable hazardous condition and planning for pre-emptive repair actions. The primary objective of this thesis is to estimate the DoS in CBM and its spatial variation by developing an inexpensive electrical impedance based non-destructive technique.

In this work, the CBM samples of 75 mm x 75 mm x 300 mm are considered which host embedded electrodes for multiple measurements along the sample length for determination of the spatial variation of the impedance as a function of the DoS. The AC voltage is applied at radio frequencies (RF) ranging from 100 kHz to 500 kHz; the reason being that low RF has higher penetration in the material due to its inverse relationship to the square root of frequency, thus able to generate information from larger depth. To generate simultaneous information corresponding to a band of frequencies, a pulse based input excitation is applied. To avoid the DC component and higher frequencies, the D-Lorentz waveform is chosen as the input waveform. The output signals are acquired in time domain in the oscilloscope and converted to frequency domain by performing FFT in the MATLAB environment. Subsequently, from the obtained FFT amplitudes at specific frequencies, the cumulative impedance between the source and at various measurement electrode positions along the length of the sample are calculated.

Two different approaches are considered to correlate DoS to the measured electrical parameters. One method is the **Voltage Ratio Method** in which the variation of the real and imaginary parts of output to input voltage ratio along the length of the sample is investigated with the DoS being homogenized along the sample through treatment in the climate chamber. It is observed that the plot between the real part and imaginary parts of the ratio vary linearly along the length for each DoS. The gradients of the lines are distinct for each DoS, thus the gradients

are used for estimation of the DoS for the homogenized sample. A second more general approach is developed which is named as the **Equivalent Circuit Method**, based on the linear variation of the cumulative real and imaginary parts of the impedance along the length for spatially homogenized DoS condition of the sample. The sample is discretized into parallel R-C circuit elements and empirical relationships between the bulk conductivity and the DoS are established for various levels of homogenized DoS during drying and wetting cycles of the CBM. The variation of the bulk relative permittivity for various frequencies is also explored and the values are found to be significantly higher than the value of the constituent ingredients. This enhanced value of relative permittivity is attributed to the Maxwell-Wagner (MW) effect in this frequency range.

For general situations, where the DoS is spatially variable in a CBM, a Tikhonov parameter and a Radial Basis Function (RBF) based inversion technique is developed that reconstructs the impedance profile along the length of the sample. The technique is observed to be robust with sparse measurement data. Further, using the empirical relationships derived from the equivalent circuit model, the impedance variation can be converted to spatial variation of the DoS. Thus, it demonstrates that DoS can be estimated from the knowledge of impedance or conductivity of the moist material. The methodology is validated by comparing the gross DoS of the sample estimated from DoS profile and gross DoS calculated from gravimetric measurement. The information obtained with this method related to DoS profile can provide preliminary data for assessment of transport property of the material which may be utilized for quality control and other important assessments of the CBM.

सार

सीमेंट आधारित सामग्री (सीबीएम) छिद्रपूर्ण हैं और सीमेंट कंक्रीट, सीमेंट मोर्टार या सीमेंट पेस्ट के रूप में निर्माण में उपयोग की जाने वाली सामग्रियों का एक महत्वपूर्ण हिस्सा है। सीबीएम की झरझरा प्रकृति छिद्रों के माध्यम से नमी की आवाजाही की सुविधा देती है जो आक्रामक रसायनों के लिए एक नाली के रूप में भी काम करती है। सभी अपमानजनक रासायनिक प्रतिक्रियाएं नमी की उपस्थिति में होती हैं जो विभिन्न स्रोतों से उत्पन्न हो सकती हैं जैसे कि वर्षा जल, सतही जल या भूजल। सामग्री की परिवहन संपत्ति और आक्रामक रसायनों के प्रसार के लिए संवेदनशीलता, संतृप्ति (DoS) की डिग्री पर निर्भर है और न केवल सकल DoS के आकलन के लिए, बल्कि सामग्री में इसके लौकिक भिन्नता और स्थानिक वितरण की जानकारी आवश्यक है। यह संभावित खतरनाक स्थिति के लिए सामग्री की भेद्यता के स्तर की पहचान करने और पूर्व-खाली मरम्मत कार्यों के लिए योजना बनाने में सक्षम बनाता है। इस थीसिस का प्राथमिक उद्देश्य सीबीएम में DoS का अनुमान लगाना और एक सस्ती विद्युत प्रतिबाधा आधारित गैर-विनाशकारी तकनीक विकसित करके इसकी स्थानिक भिन्नता है।

इस काम में, 75 मिमी x 75 मिमी x 300 मिमी के सीबीएम नमूनों पर विचार किया जाता है, जो कि DoS के एक फ़ंक्शन के रूप में प्रतिबाधा के स्थानिक भिन्नता के निर्धारण के लिए नमूना लंबाई के साथ कई मापों के लिए एम्बेडेड इलेक्ट्रोड की मेजबानी करता है। इसी वोल्टेज 100 kHz से 500 kHz तक के रेडियो आवृत्तियों (RF) पर लगाया जाता है; कारण यह है कि निम्न RF आवृत्ति के वर्गमूल से इसके विपरीत संबंध के कारण सामग्री में उच्च पैठ रखता है, इस प्रकार यह बड़ी गहराई तक जानकारी उत्पन्न करने में सक्षम है। आवृत्तियों के एक बैंड के साथ एक साथ सूचना उत्पन्न करने के लिए, एक पल्स आधारित इनपुट उत्तेजना लागू की जाती है। डीसी घटक और उच्च आवृत्तियों से बचने के लिए, डी-लोरेन्ज़ तरंग को इनपुट तरंग के रूप में चुना जाता है। आउटपुट सिग्नल ऑसिलोस्कोप में समय डोमेन में प्राप्त किए जाते हैं और MATLAB वातावरण में FFT प्रदर्शन करके आवृत्ति डोमेन में परिवर्तित होते हैं। इसके बाद, विशिष्ट आवृत्तियों पर प्राप्त एफएफटी आयामों से, स्रोत के बीच और नमूना की लंबाई के साथ विभिन्न माप इलेक्ट्रोड पदों पर संचयी प्रतिबाधा की गणना की जाती है।

दो अलग-अलग दृष्टिकोणों को मापा विद्युत मापदंडों के लिए DoS को सहसंबंधित माना जाता है। एक विधि वोल्टेज अनुपात विधि है जिसमें नमूना की लंबाई के साथ आउटपुट वोल्टेज के अनुपात में वास्तविक और काल्पनिक भागों की भिन्नता की जांच की जाती है, जिसमें DoS को जलवायु कक्ष में उपचार के माध्यम से नमूने के साथ समरूप किया जाता है। यह देखा गया है कि अनुपात के वास्तविक भाग और काल्पनिक भागों के बीच का भूखंड प्रत्येक DoS की लंबाई के साथ रैखिक रूप से भिन्न होता है। लाइनों के ग्रेडिएंट प्रत्येक DoS के लिए अलग होते हैं, इस प्रकार ग्रेडिएंट्स

Homogenized नमूने के लिए DoS के अनुमान के लिए उपयोग किया जाता है। एक और अधिक सामान्य दृष्टिकोण विकसित किया गया है जिसे नमूना के स्थानिक रूप से समरूपित DoS स्थिति के लिए लंबाई के साथ प्रतिबाधा के संचयी वास्तविक और काल्पनिक भागों के रैखिक भिन्नता के आधार पर समतुल्य सर्किट विधि के रूप में नामित किया गया है। नमूना को समानांतर आर-सी सर्किट तत्वों और बल्क चालकता के बीच अनुभवजन्य संबंधों में विवेकाधीन किया जाता है और CBM के सूखने और गीला होने के दौरान DoS को विभिन्न स्तर के समरूप डीओएस के लिए स्थापित किया जाता है। विभिन्न आवृत्तियों के लिए थोक सापेक्ष पारगम्यता की भिन्नता का भी पता लगाया जाता है और मूल्यों को घटक अवयवों के मूल्य से काफी अधिक

पाया जाता है। इस क्रमिक सीमा में मैक्सवेल-वैगनर (MW) प्रभाव के लिए सापेक्ष पारगम्यता के इस संवर्धित मूल्य को जिम्मेदार ठहराया गया है।

सामान्य परिस्थितियों के लिए, जहां CS में DoS स्थानिक रूप से परिवर्तनशील होता है, एक Tikhonov पैरामीटर और एक रेडियल बेसिस फ़ंक्शन (RBF) आधारित इनवर्जन तकनीक विकसित की जाती है जो नमूना की लंबाई के साथ प्रतिबाधा प्रोफ़ाइल को फिर से संगठित करती है। तकनीक को विरल माप डेटा के साथ मजबूत होने के लिए मनाया जाता है। इसके अलावा, समतुल्य सर्किट मॉडल से प्राप्त अनुभवजन्य संबंधों का उपयोग करते हुए, प्रतिबाधा भिन्नता को DoS की स्थानिक भिन्नता में परिवर्तित किया जा सकता है। इस प्रकार, यह दर्शाता है कि DoS को नम सामग्री के प्रतिबाधा या चालकता के ज्ञान से अनुमानित किया जा सकता है। DoS प्रोफ़ाइल से अनुमानित नमूने के सकल DoS की तुलना करके और Gravimetric माप से गणना की सकल DoS द्वारा कार्यप्रणाली को मान्य किया गया है। DoS प्रोफ़ाइल से संबंधित इस पद्धति से प्राप्त जानकारी सामग्री की परिवहन संपत्ति के मूल्यांकन के लिए प्रारंभिक डेटा प्रदान कर सकती है, जिसका उपयोग गुणवत्ता नियंत्रण और CBM के अन्य महत्वपूर्ण आकलन के लिए किया जा सकता है।

Contents

List of Figures	x
List of Tables	xxi
List of Symbols.	xxii
List of Acronyms	xxv
1 Introduction	1
1.1 General.	1
1.2 Durability issue of cement based materials	1
1.3 Role of moisture in degradation.	2
1.4 Relationship between transport phenomenon and DoS	3
1.5 Preview of moisture measuring techniques	4
1.6 Organization of the Thesis	5
2 Theoretical background and Literature Review	6
2.1 Background.	6
2.2 Moisture mobility in CBM.	9
2.3 Response of CBM under EM field.	10
2.4 Bulk conductivity at low RF.	13

2.5 Bulk permittivity at low RF.	16
2.6 Conductivity and Permittivity measuring techniques	19
2.6.1 Resistivity Measurements	19
2.6.2 AC impedance Measurements	20
2.6.3 Tomographic Method of Measurement	21
2.6.4 Time domain reflectometry (TDR)	24
2.6.5 Ground Penetrating Radar (GPR) techniques	25
2.7 Summary and Inferences	27
2.8 Objective and Scope.	28
2.8.1 Gap in Research.	28
2.8.2 Research Objective.	29
2.8.3 Scope of Research	29
3 Experimental Investigation.	31
3.1 General.	31
3.2 Conceptualization and Development of Set-up	31
3.3 Materials Used and Sample Preparation	33
3.4 Sample Conditioning.	35
3.5 Data Acquisition and Processing.	37
3.5.1 Real and Imaginary parts of impedance	39
3.6 Summary.	40
4 Degree of Saturation (DoS) for Homogenized Sample.	42
4.1 General.	42
4.2 Voltage Ratio Method (VRM)	42

4.3	Equivalent Circuit Method (ECM)	47
4.3.1	Statistical analysis of output	49
4.3.2	Linear variation of impedance.	51
4.3.3	Properties of cement paste.	53
4.3.3.1	Impedance of cement paste.	53
4.3.3.2	Bulk conductivity of cement paste.	55
4.3.3.3	Bulk permittivity of cement paste.	61
4.3.4	Properties of cement mortar.	62
4.3.4.1	Impedance of cement mortar.	62
4.3.4.2	Bulk conductivity of cement mortar.	65
4.3.4.3	Bulk permittivity of cement mortar.	68
4.3.5	Properties of cement concrete.	71
4.3.5.1	Impedance of cement concrete.	71
4.3.5.2	Bulk conductivity of cement concrete.	73
4.3.5.3	Bulk permittivity of cement concrete.	77
4.3.6	Comparison of electrical properties of CBM.	80
4.4	Summary	82
5	Inversion Based Determination of DoS.	83
5.1	General.	83
5.2	Background.	83
5.3	Definition of RBF.	84
5.4	Formulation of inverse problem.	87
5.5	The inversion technique.	89
5.5.1	Selection of suitable shape parameter and number of RBFs.	92
5.5.2	Flow chart of the inversion procedure	94

5.6	Inversion applied to homogenized sample.	96
5.6.1	Regularization parameter from L-curve.	96
5.6.2	Cumulative fit for impedance.	97
5.6.3	Fit for impedance distribution.	98
5.6.4	Distribution of bulk conductivity.	101
5.6.5	Distribution of relative bulk permittivity.	102
5.7	Fit for non-homogenized sample.	103
5.7.1	Fitting of cumulative impedance.	104
5.7.2	Leave One Out Cross Validation (LOOCV)	107
5.7.3	Distribution of impedance	109
5.7.4	Distribution of bulk conductivity.	111
5.7.5	Distribution of bulk relative permittivity.	112
5.8	Mapping of spatial distribution of DoS.	113
5.9	Summary	115
6	Conclusions.	117
6.1	General.	117
6.2	Main contributions.	119
6.3	Future research.	120
	References.	121
	Research Publications from this work	133
	Appendix-A.	134
	Figures and tables of conductivity and DoS	134
	Brief biodata of the author.	135

List of Figures

1.1	Damage due to a) carbonation of concrete and b) corrosion of reinforcement.	3
1.2	Damage due to a) growth of mold and b) efflorescence.	3
2.1	Distribution of charge in normal condition (left), polarization of charge under electric field (right) in porous CBM	11
2.2	Dielectric dispersion of porous materials in low radio frequency	12
2.3	Schematic of the parameters used to describe electrical measurements in porous materials for (a) resistivity of the pore solution (b) porosity and (c) connectivity	14
2.4	Representation of Electrical double layer	15
2.5	Representation of various phases present in partially saturated porous material and normal components of electric field	16
2.6	Equivalent circuit for cement paste employed by Cabeza et al	20
2.7	TDR set up for soil moisture determination	24
2.8	Configuration of radar measurement	26
2.9	Impedance Spectra of Cement paste under various DoS	28
3.1	Experimental set up with mortar sample.	32
3.2	a) Time domain input signal and response at various DoS; b) frequency spectrum of the signals.	32
3.3	Mold for specimen preparation with placement of electrodes.	34
3.4	Experimental sample cement paste (bottom), cement mortar (middle) and concrete (top) with orientation of electrodes.	35
3.5	a) Wrapping of samples for condition b) Conditioning chamber with set	

temperature 27°C and relative humidity 65% for storing samples.	36
3.6 Schematic of experimental set up.	37
4.1 Error bar showing spread of 95% confidence interval of a) real and b) imaginary parts of ratio of output voltage and input voltage (V_k/V_{in}) at 100 kHz frequency for MM60 sample in drying cycle	42
4.2 Polar plot of real vs imaginary parts of voltage ratio $\frac{V_k(\omega)}{V_{in}(\omega)}$ under various DoS and the their linear fit along the length for CC45 in a) drying cycle and b) wetting cycle at excitation frequency 100 kHz.	43
4.3 Polar plot of real vs imaginary parts of voltage ratio $\frac{V_k(\omega)}{V_{in}(\omega)}$ under various DoS and the their linear fit along the length in drying cycle for a) MM60 b) MM70 at excitation frequency 300 kHz.	44
4.4 Relationship between DoS and angle for estimation of the DoS (β) for CC45 at excitation frequency a) 75 kHz and b) 100 kHz.	45
4.5 Relationship between DoS and angle for estimation of the DoS for MM45 at excitation frequency a) 100 kHz and b) 150 kHz.	46
4.6 Relationship between DoS and angle for estimation of the DoS at excitation frequency 100 kHz for a) CC55 and b) CC65.	47
4.7 Basic circuit model for the CBM.	48
4.8 Variation of real and imaginary parts of impedance with distance for various DoS of MM45 sample at 300 kHz.	48
4.9 Error bar showing spread of 95% confidence interval of real and imaginary	

parts of ratio of output voltage and voltage across the resistance (V_k/V_e) at 300 kHz frequency for CC45 sample.	50
4.10 Error bar showing spread of 95% confidence interval of real and imaginary parts of ratio of output voltage and voltage across the resistance (V_k/V_e) at 300 kHz frequency for MM45 sample.	50
4.11 Linear variation of cumulative values of real and imaginary parts of the impedance for CC45 sample under various DoS for excitation frequency 300 kHz.	51
4.12 Variation of coefficient of determination (R^2) value of linear fit of cumulative real and imaginary parts of impedance for MM45 wetting cycle samples under various DoS for excitation frequency 300 kHz.	52
4.13 Variation of coefficient of determination (R^2) value of linear fit of cumulative real and imaginary parts of impedance for CC45 drying cycle samples under various DoS for excitation frequency 300 kHz.	52
4.14 Real and imaginary parts of impedance for CP40 (left) and CP45 (right)for different DoS and frequencies in wetting cycle.	54
4.15 Variation of a) real part and b) imaginary part of impedance with DoS for cement paste at 300 kHz under wetting cycle.	55
4.16 Bulk conductivity(σ) of cement paste a) CP40 and b) CP45 under different DoS and frequencies in wetting cycle.	56
4.17 Bulk conductivity variation with DoS for cement paste at100 kHz under	

wetting cycle.	56
4.18 Bulk conductivity variation with DoS for Cement paste at 300 kHz under wetting cycle.	57
4.19 Bulk conductivity variation with DoS for Cement paste at 500 kHz under wetting cycle.	58
4.20 Relationship between bulk conductivity and DoS for Cement paste at 300 kHz in wetting cycle a) polynomial fit b) logarithmic fit	60
4.21 Bulk relative permittivity (ϵ_r) of cement paste a) CP40 and b) CP45 under different DoS and frequencies under wetting cycle.	61
4.22 Bulk relative permittivity(ϵ_r) variation with DoS for cement paste at excitation frequency a) 100 kHz and b) 300 kHz under wetting cycle.	62
4.23 Real and imaginary parts of impedance for MM45 under different DoS and frequencies indrying and wetting cycles.	63
4.24 Variation of a) real part and b) imaginary part of impedance with DoS for cement mortar (MM45) at 300 kHz under drying and wetting cycles.	63
4.25 Variation of a) real part and b) imaginary part of impedance with DoS for cement mortar (MM60) at 300 kHz under drying and wetting cycles.	64
4.26 Variation of a) real part and b) imaginary part of impedance with DoS for cement mortar (MM70) at 300 kHz under drying and wetting cycles.	64
4.27 Bulk conductivity(σ) of cement mortar (MM45) under different DoS and frequencies a) in drying and b) wetting cycle.	65

4.28 Bulk conductivity(σ) of cement mortar (MM60) under different DoS and frequencies a) in drying and b) wetting cycle.	66
4.29 Bulk conductivity of(σ) cement mortar (MM70) under different DoS and frequencies a) in drying and b) wetting cycle.	66
4.30 Relationship between bulk conductivity and DoS for cement mortar (MM45) in drying and wetting cycles at 300 kHz excitation frequency a) polynomial fit and b) logarithmic fit	67
4.31 Relationship between bulk conductivity and DoS for cement mortar (MM60) in drying and wetting cycles at 300 kHz excitation frequency a) polynomial fit and b) logarithmic fit	67
4.32 Relationship between bulk conductivity and DoS for cement mortar (MM70) in drying and wetting cycles at 300 kHz excitation frequency a) polynomial fit and b) logarithmic fit	67
4.33 Bulk relative permittivity(ϵ_r)of cement mortar (MM45) under different DoS and frequencies a) in drying and b) wetting cycle.	69
4.34 Bulk relative permittivity(ϵ_r)of cement mortar (MM60) under different DoS and frequencies a) in drying and b) wetting cycle.	69
4.35 Bulk relative permittivity(ϵ_r)of cement mortar (MM70) under different DoS and frequencies a) in drying and b) wetting cycle.	70
4.36 Bulk relative permittivity (ϵ_r) variation with DoS for cement mortar at excitation frequency 300 kHz under drying and wetting cycle.	71

4.37	Real and imaginary parts of impedance for CC55 under different DoS and frequencies in drying and wetting cycles.	72
4.38	Variation of a) real part and b) imaginary part of impedance with DoS for cement concrete at 300 kHz under drying and wetting cycles.	72
4.39	Bulk conductivity(σ) of concrete (CC45) under different DoS and frequencies a) in drying and b) wetting cycle.	73
4.40	Bulk conductivity(σ) of concrete (CC55) under different DoS and frequencies a) in drying and b) wetting cycle.	74
4.41	Bulk conductivity(σ) of concrete (CC65) under different DoS and frequencies a) in drying and b) wetting cycle.	74
4.42	Relationship between bulk conductivity and DoS for cement concrete (CC45) in drying and wetting cycles at 300 kHz excitation frequency a) polynomial fit and b) logarithmic fit	75
4.43	Relationship between bulk conductivity and DoS for cement concrete (CC55) in drying and wetting cycles at 300 kHz excitation frequency a) polynomial fit and b) logarithmic fit	76
4.44	Relationship between bulk conductivity and DoS for cement concrete (CC65) in drying and wetting cycles at 300 kHz excitation frequency a) polynomial fit and b) logarithmic fit	76
4.45	Bulk relative permittivity(ϵ_r) of concrete (CC45) under different DoS and frequencies a) in drying and b) wetting cycle.	77

4.46 Bulk relative permittivity(ϵ_r)of concrete (CC55) under different DoS and frequencies a) in drying and b) wetting cycle.	78
4.47 Bulk relative permittivity(ϵ_r)of concrete (CC65) under different DoS and frequencies a) in drying and b) wetting cycle.	78
4.48 Bulk relative permittivity(ϵ_r) variation with DoS for cement concrete at excitation frequency 300 kHz under drying and wetting cycle.	79
4.49 Bulk relative permittivity(ϵ_r) variation with DoS for cement concrete at excitation frequency 1 MHz under drying and wetting cycle.	80
5.1 Impedance distribution along the length.	84
5.2 The common types of Radial Basis Functions (RBFs) with a constant shape parameter over a constant length.	85
5.3 Variation of shape of a) Gaussian RBF and b) Multiquadric RBF with respect to change of shape parameter.	86
5.4 Multiple RBFs (n number) in the computational domain with equally spaced support points (μ) of a) GA-RBF b) MQ-RBF c)IMQ-RBF and d) SG-RBF.	87
5.5 Evolution of L-curve a) For a long range of λ showing steep part and flat part b) For short range of λ showing the vertex of L-curve.	91
5.6 Evolution of L-curves a) with variation of number of RBF having shape parameter (s=0.075) b) with variation of shape parameter having number of RBF (n=601)	93

5.7	L-curves for different DoS of CC45 under excitation frequency 300 kHz	
	for a) drying cycle and b) wetting cycle.	96
5.8	Fit of real and imaginary parts of cumulative impedance of CC45 under	
	300 kHz excitation frequency using GA-RBF and IMQ-RBF for DS87.5	
	(left) and DS62.5 (right)	97
5.9	Fit of real and imaginary parts of cumulative impedance of CC45 at	
	300 kHz excitation frequency for DS100 and DS87.5 using GA-RBF	
	in a) drying cycle and b) wetting cycle.	98
5.10	Fit of real and imaginary parts of cumulative impedance of CC45	
	under 300 kHz excitation frequency for DS75 and DS62.5 using	
	GA-RBF in a) drying cycle and b) wetting cycle.	98
5.11	Reconstruction of distribution of real and imaginary parts of impedance	
	a) real part in drying cycle b) imaginary part in drying cycle c) real part	
	in wetting cycle d) imaginary part in wetting cycle using GA-RBF.	99
5.12	Reconstruction of distribution of real and imaginary parts of impedance	
	a) real part in drying cycle b) imaginary part in drying cycle c) real part in	
	wetting cycle d) imaginary part in wetting cycle using IMQ-RBF.	99
5.13	Assumed circuit in elemental length of dx	101
5.14	Reconstruction of distribution of bulk conductivity (σ) of CC45 at	
	300 kHz frequency in the drying cycle a) using GA-RBF and	
	b) using IMQ-RBF.	101

5.15	Reconstruction of distribution of bulk conductivity (σ) of CC45 under 300 kHz frequency in the wetting cycle a) using GA-RBF and b) using IMQ-RBF.	102
5.16	Reconstruction of distribution of bulk relative permittivity (ϵ_r) of CC45 for different DoS under 300 kHz frequency in drying cycle a) using GA-RBF b) using IMQ-RBF.	102
5.17	Reconstruction of distribution of bulk relative permittivity (ϵ_r) of CC45 for different DoS under 300 kHz frequency in wetting cycle a) using GA-RBF b) using IMQ-RBF.	103
5.18	Schematic representation of specimen kept for inducing spatial variation of moisture.	104
5.19	Predicted curves showing real and imaginary parts of cumulative impedance for CC45 at 300 kHz frequency under L1 saturation level a) sample 1 and b) sample 2 using GA-RBF and IMQ-RBF.	105
5.20	Predicted curves showing real and imaginary parts of cumulative impedance under L1 saturation level a) sample 1 of CC65 and b) sample 2 of CC65 at 300 kHz frequency using GA-RBF and IMQ-RBF.	105
5.21	Approximation of cumulative impedance using IMQ-RBF for LOOCV for sample 1 of CC45 under saturation level L1at 300 kHz a) real part b) imaginary part.	107

5.22	Approximation of cumulative impedance using IMQ-RBF for LOOCV for sample 2 of CC45 under saturation level L1 at 300 kHz a) real part b) imaginary part.	108
5.23	Distribution of real and imaginary parts of impedance for CC45 at 300 kHz frequency under variable moisture condition a) sample 1 and b) sample 2.	109
5.24	Distribution of real and imaginary parts of impedance for CC65 under variable moisture condition a) sample 1 and b) sample 2.	110
5.25	Comparison of distribution of bulk conductivity (σ) for CC45 at 300 kHz frequency for L1 and L2 saturation level for a) sample 1 and b) sample 2.	111
5.26	Distribution of bulk relative permittivity (ϵ_r) obtained for CC45 at 300 kHz frequency under L1 and L2 saturation level for a) sample 1 and b) sample 2.	112
5.27	Estimation of DoS profile from bulk conductivity value a) Sample 1 and 2 of CC45 for L2 saturation and b) Sample 1 and 2 of CC65 for L1 saturation.	114
a.	Relationship between bulk conductivity and DoS for cement concrete (CC45) in drying and wetting cycles at 100 kHz excitation frequency.	134
b.	Relationship between bulk conductivity and DoS for cement concrete (CC55) in drying and wetting cycles at 100 kHz excitation frequency.	134

c. Relationship between bulk conductivity and DoS for cement concrete	
(CC65) in drying and wetting cycles at 100 kHz excitation frequency.	135
d. Relationship between bulk conductivity and DoS for cement concrete	
(CC45) in drying and wetting cycles at 500 kHz excitation frequency.	136
e. Relationship between bulk conductivity and DoS for cement concrete	
(CC55) in drying and wetting cycles at 500 kHz excitation frequency.	136
f. Relationship between bulk conductivity and DoS for cement concrete	
(CC65) in drying and wetting cycles at 500 kHz excitation frequency.	137
g. Relationship between bulk conductivity and DoS for cement mortar	
(MM45) in drying and wetting cycles at 100 kHz excitation frequency.	138
h. Relationship between bulk conductivity and DoS for cement mortar	
(MM60) in drying and wetting cycles at 100 kHz excitation frequency.	138
k. Relationship between bulk conductivity and DoS for cement mortar	
(MM70) in drying and wetting cycles at 100 kHz excitation frequency.	139
l. Relationship between bulk conductivity and DoS for cement mortar	
(MM45) in drying and wetting cycles at 500 kHz excitation frequency.	140
m. Relationship between bulk conductivity and DoS for cement mortar	
(MM60) in drying and wetting cycles at 500 kHz excitation frequency.	140
n. Relationship between bulk conductivity and DoS for cement mortar	
(MM70) in drying and wetting cycles at 500 kHz excitation frequency.	141

List of Tables

2.1 Description of pores in CBM	10
2.2 Various saturation regimes of granular unbonded porous materials with DoS.	17
3.1 Details of the specimen for the experimental programme.	33
3.2 Water absorption coefficient of CBM in percentage.	36
4.1 Values of coefficients for determination of DoS for cement paste at 300 kHz	60
4.2 Values of coefficients for determination of DoS for mortar at 300 kHz	68
4.3 Values of coefficients for determination of DoS for concrete at 300 kHz	77
5.1 Common types of radial basis function.	85
5.2 Comparison of the real and imaginary parts of impedance per unit length obtained from the linear fit and the inversion approach for CC45 for various DoS at a frequency of 300 kHz.	100
5.3 RMS error of approximation (ϵ_1) with GA-RBF and IMQ-RBF.	106
5.4 Maximum error of approximation (ϵ_2) with GA-RBF and IMQ-RBF.	106
5.5 Error of approximation using IMQ-RBF for leaving one out data for sample S1L1-CC45 at 300 kHz frequency.	108
5.6 Comparison of DoS value obtained gravimetrically and from the technique presented in this study.	115
a. Values of coefficients for determination of DoS for concrete at 100 kHz	135
b. Values of coefficients for determination of DoS for concrete at 500 kHz	137
c. Values of coefficients for determination of DoS for mortar at 100 kHz	139
d. Values of coefficients for determination of DoS for mortar at 500 kHz	141

List of Symbols

Symbol	Description
L_k	Length of the specimen from source to k^{th} electrode
R_e	Resistance of the external resistor
S_w	Degree of saturation
V_e	Voltage drop across external resistor
V_{in}	Input voltage
V_k	Output voltage at k^{th} electrode
V_r^i	Imaginary part of output to input voltage
V_r^r	Real part of output to input voltage
Z^i	Imaginary Part of cumulative impedance
Z_{int}^1	Interfacial impedance in source end
Z_{int}^2	Interfacial impedance in far end
Z_{int}^{i1}	Imaginary part of interfacial impedance in source end
Z_{int}^{i2}	Imaginary part of interfacial impedance in far end
Z_{int}^{r1}	Real part of interfacial impedance in source end
Z_{int}^{r2}	Real part of interfacial impedance in far end
Z_k	Cumulative impedance upto k^{th} electrode
Z_k^i	Imaginary part of cumulative impedance upto k^{th} electrode
Z_k^r	Real part of cumulative impedance upto k^{th} electrode
Z^r	Real part of cumulative impedance
c_m	Velocity of electromagnetic wave in the material

m_d	Weight of dry sample
m_i	Weight of sample in any intermediate saturation level
m_s	Weight of saturated sample
z^i	Imaginary part of impedance per unit length
z^r	Real part of impedance per unit length
ε^*	Complex permittivity
ε_0	Vacuum permittivity
ε_m	Relative permittivity of the material
ε_r	Bulk relative permittivity
μ^*	Complex magnetic permeability
μ_r	Relative magnetic permeability
ρ_0	Resistivity of the pore solution
σ^*	Complex conductivity
σ_t	Total bulk conductivity
σ_w	Pore water conductivity
$\emptyset$	Porosity of the material
A	Cross sectional area of specimen
C	Capacitance
F	Formation factor
I	Current
L	Length of the specimen
R	Resistance
WA	Water absorption coefficient
c	Velocity of electromagnetic wave in free space

l	Length of waveguide
s	Shape parameter
t	Travel time of electromagnetic wave
α	Connectivity of pores
β	Angular parameter for determination of DoS
ε	Bulk permittivity
λ	Tikhonov regularization parameter
μ	Support point of radial basis function
ρ	Bulk resistivity
σ	Bulk conductivity
φ	Radial basis function
ω	Angular frequency

List of Acronyms

Acronym	Definition
AC	Alternating Current
CBM	Cement Based Material
DC	Direct Current
DoS	Degree of (Moisture) Saturation
ECM	Equivalent Circuit Method
FFT	Fast Fourier Transform
GA	Gaussian
GPR	Ground Penetrating Radar
IMQ	Inverse Muliquadric
kHz	kilo Hertz
KVL	Kirchhoff's Voltage Law
MHz	Mega Hertz
M-W	Maxwell-Wagner
NMR	Nuclear Magnetic Resonance
RBF	Radial Basis Function
RF	Radio Frequency
RH	Relative Humidity
TDR	Time Domain Reflectometry
VRM	Voltage Ratio Method
w/c	Water to Cement Ratio